

Material transport in the frame of PSI

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with contributions from many colleagues (credits inside)

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Overview and rationale

Material transport processes

Particle collisions

Plasma turbulence

Experiments

Phenomenological observations

Specific experiments

Summary and outlook

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Summary and outlook

What are the basic ingredients of material migration?

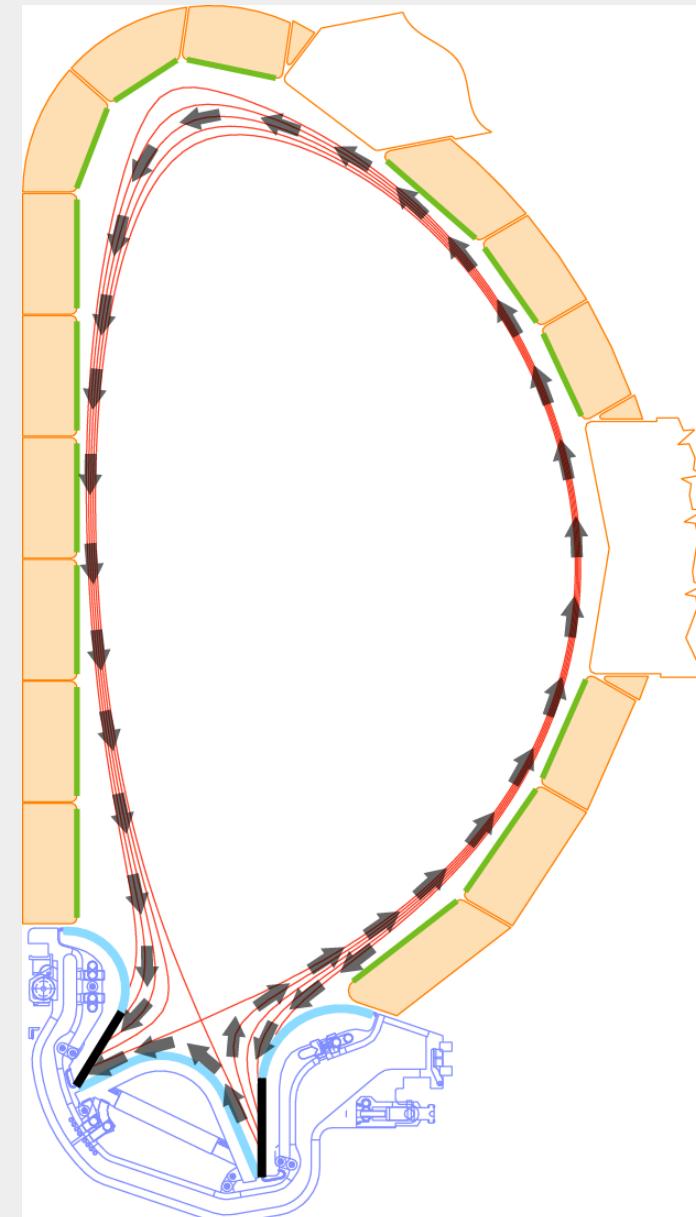
IPP

Plasma

Fuel ions + atoms (charge exchange) +
impurity ions bombard 1st wall

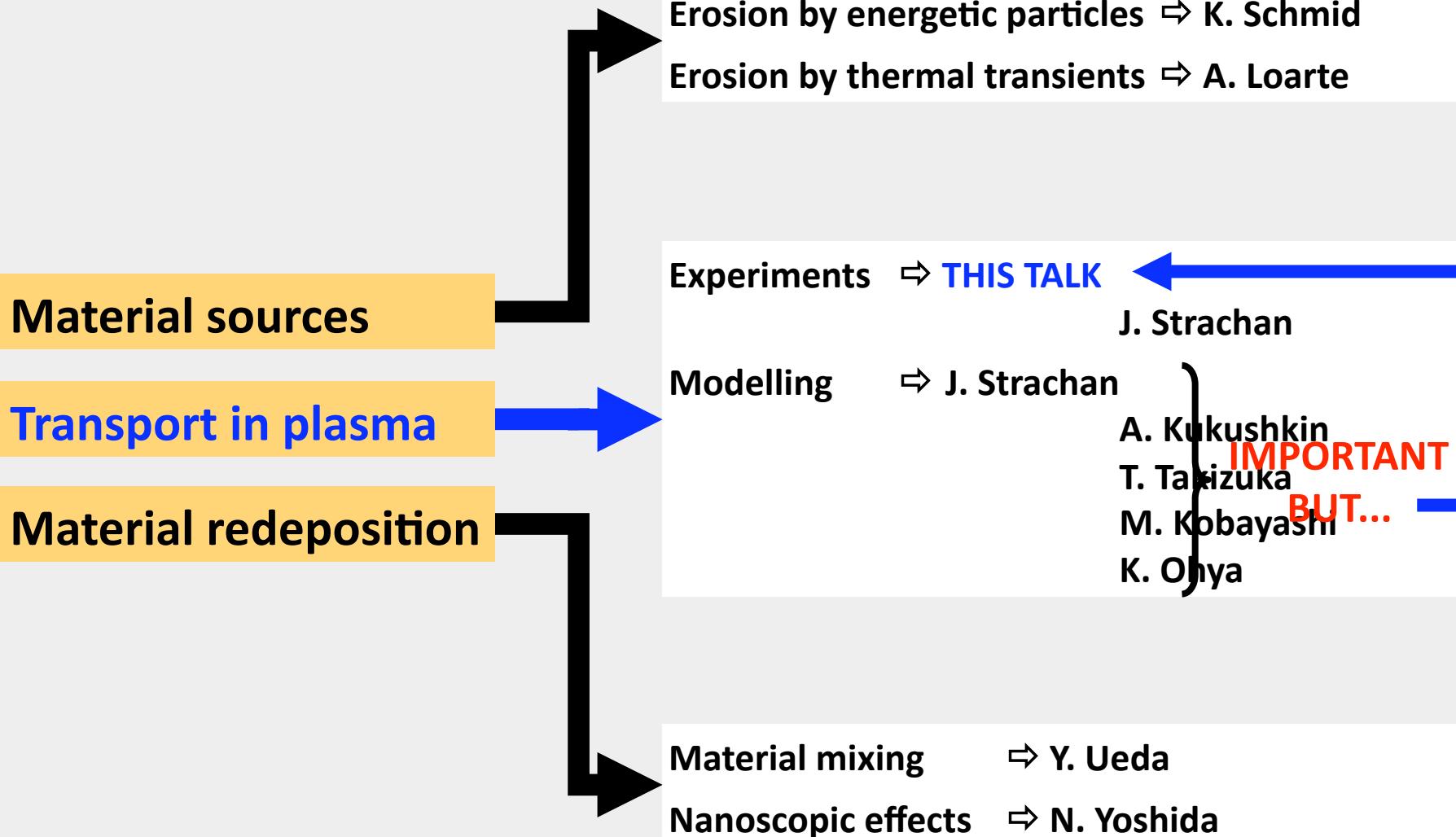
Wall materials

Erosion → Transport → Deposition
Re-erosion



What's the connection to the other lectures?

IPP

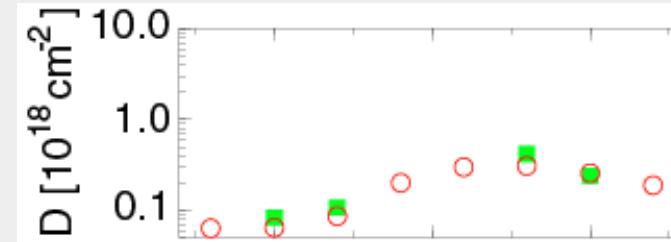
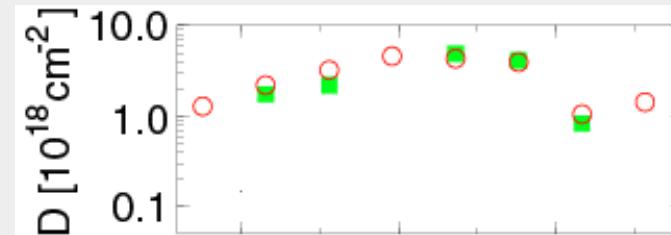
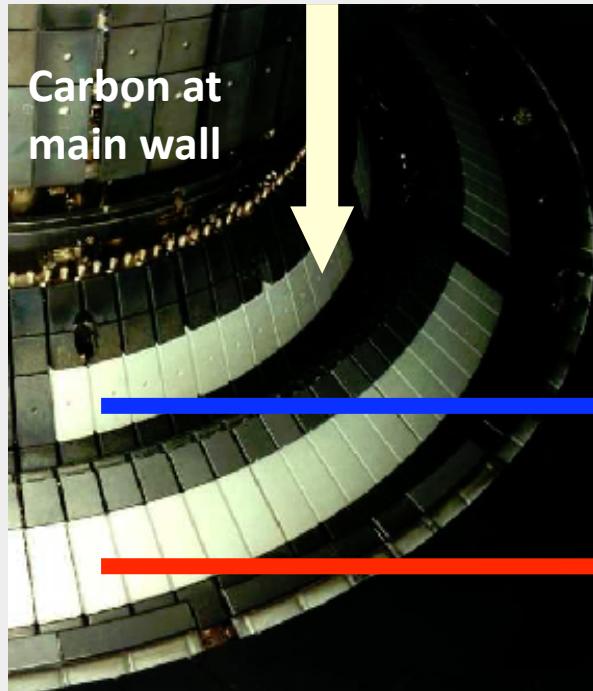


What are the consequences of material migration?

IPP

**Layer deposition and
material mixing!**

Freshly installed tungsten
divertor in ASDEX Upgrade



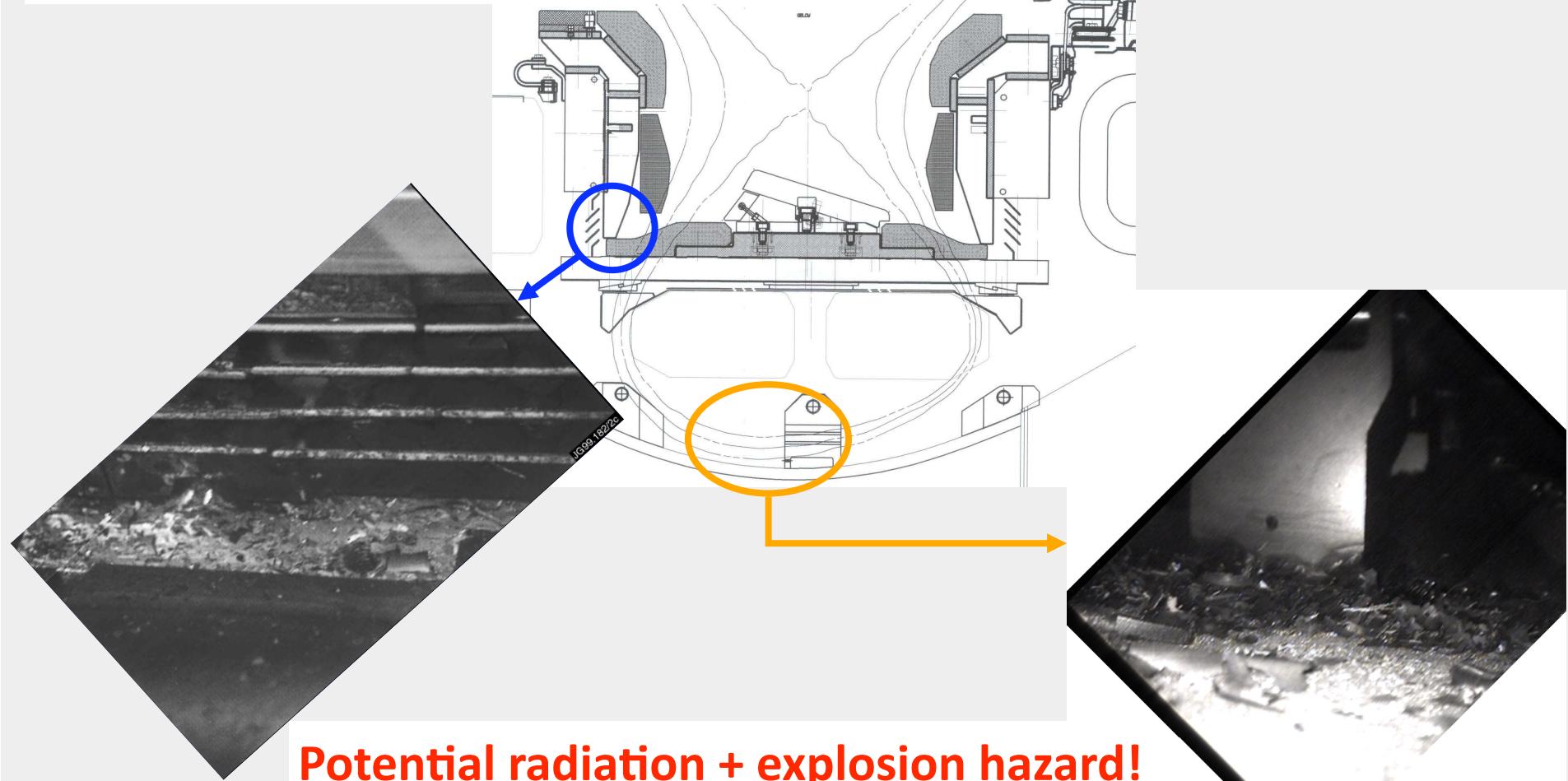
Deposited layers may form ever growing inventory of buried fuel!

What happens if deposited layers become too thick?

IPP

Layers delaminate and flake off, forming radioactive and chemically reactive dust

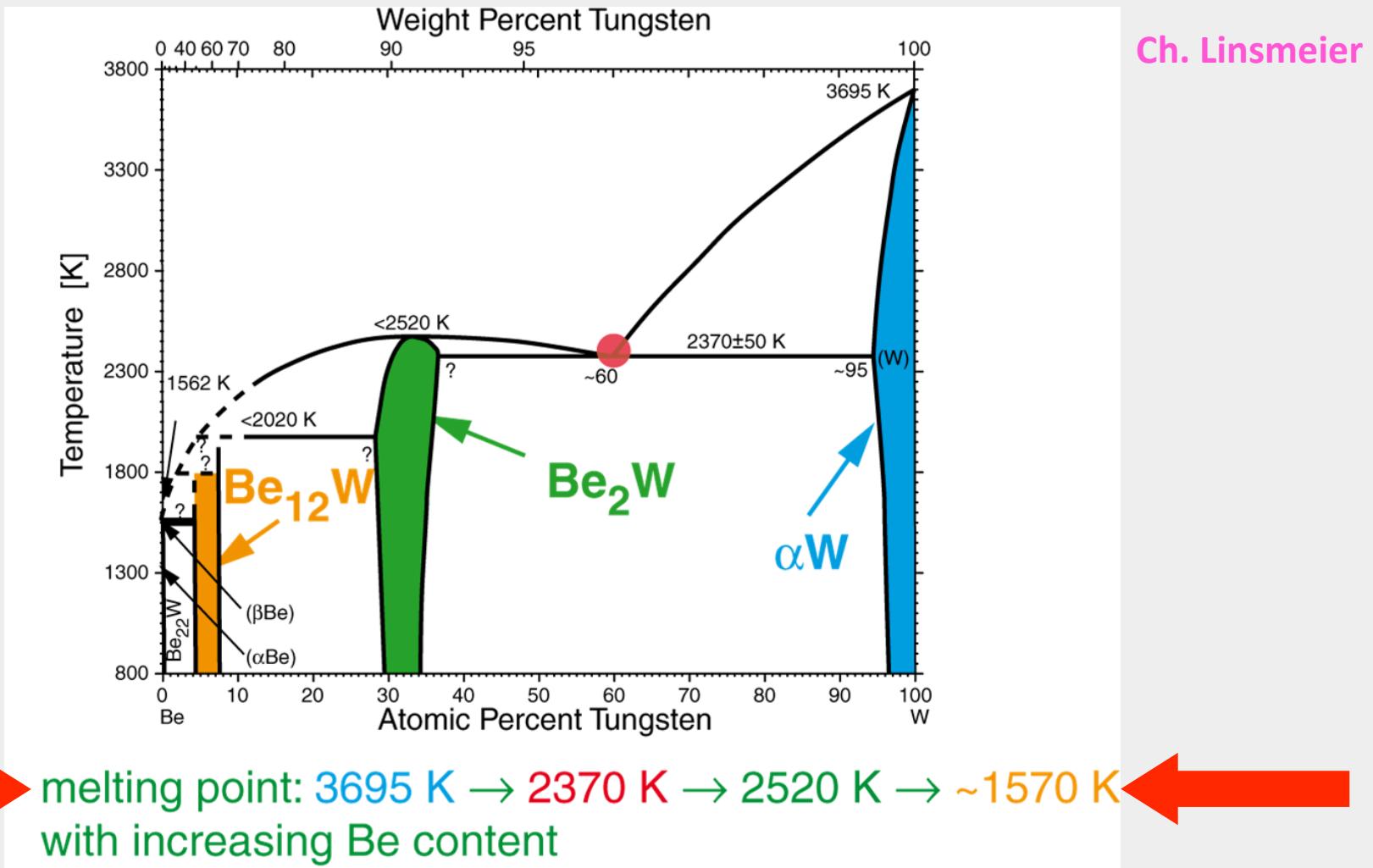
S. Brezinsek



Negative consequences of material mixing?

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YES! Example: beryllium and tungsten can form alloys



Overview and rationale

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Key questions of material (impurity) transport

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For given impurity edge density,
what is the impurity density in the plasma centre?

or

What is the impurity residence time compared to
the fuel ion residence time in the plasma?

Core transport coefficients

For given material erosion source,
how much gets into the confined plasma?

Screening factor, divertor retention

Where are eroded impurities re-deposited?

Migration paths

Impurity transport $\perp B$ by particle collisions

IPP

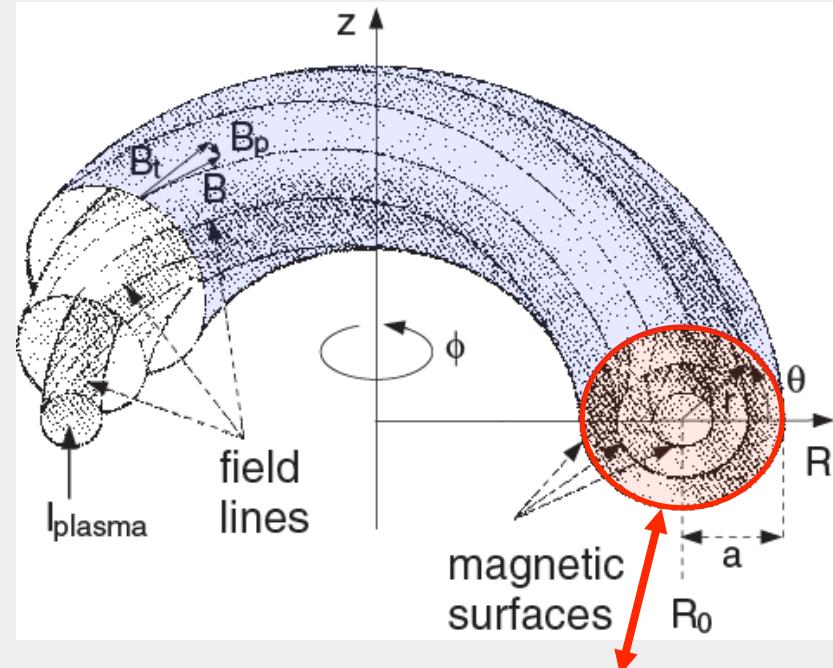
Particle conservation

$$\frac{\partial n_{I,Z}}{\partial t} = -\nabla \cdot \Gamma_{I,Z} + Q_{I,Z}$$

Ions bound to flux surface

$$\langle n_I \rangle = n_I$$

i.e. densities constant on flux surface



Impurity density is only a function of **flux surface label**

$$r = \sqrt{V/(2\pi^2 R_0)}$$

and flux is described by **diffusion + convection**

$$\frac{\partial n_{I,Z}}{\partial t} = \frac{1}{r} \frac{\partial}{\partial r} r \left(D^* \frac{\partial n_{I,Z}}{\partial r} - v^* n_{I,Z} \right) + Q_{I,Z}$$

Transport coefficients \Rightarrow averages over flux surface

Impurity transport $\perp \mathbf{B}$ by particle collisions



$$D = D^{CL} + D^{PS} + D^{BP}$$

$$D^{CL} \cong \frac{m_I k T v_{ID}}{B_0^2 e^2 Z^2} \propto \frac{1}{\sqrt{T} B_0^2 Z^2}$$

Classical transport
due to collisional friction forces $\perp \mathbf{B}$

$$D^{PS} \cong 2q^2 D^{CL} \propto \frac{1}{\sqrt{T} B_p^2 Z^2}$$

Pfirsch-Schlüter transport
due to collisional friction forces $\parallel \mathbf{B}$

$$D^{BP} \cong \frac{q^2}{\varepsilon^2} \frac{k T \mu_{ID}^*}{B_0^2 e^2 Z n_I} \propto \frac{1}{\sqrt{T} B_p^2 Z n_I}$$

Banana-Plateau transport
due to viscosity forces $\parallel \mathbf{B}$

$$\varepsilon = \frac{r}{R_0}$$

$$q = \varepsilon \frac{B_T}{B_P}$$

Impurity transport $\perp B$ by particle collisions

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$$V = V^{CL} + V^{PS} + V^{BP}$$

$$V^{XX} = D^{XX} Z \left(\frac{d \ln n_D}{dr} + H^{XX} \frac{d \ln T}{dr} \right)$$

All drifts have the same form but
the sign of H^{XX} may change!

Why is this important?

$$\frac{d \ln n_Z}{dr} = Z \frac{d \ln n_I}{dr} \left(1 + H_{eff} \frac{d \ln T}{dr} \Big/ \frac{d \ln n_I}{dr} \right)$$



Temperature screening factor \Rightarrow generally negative!

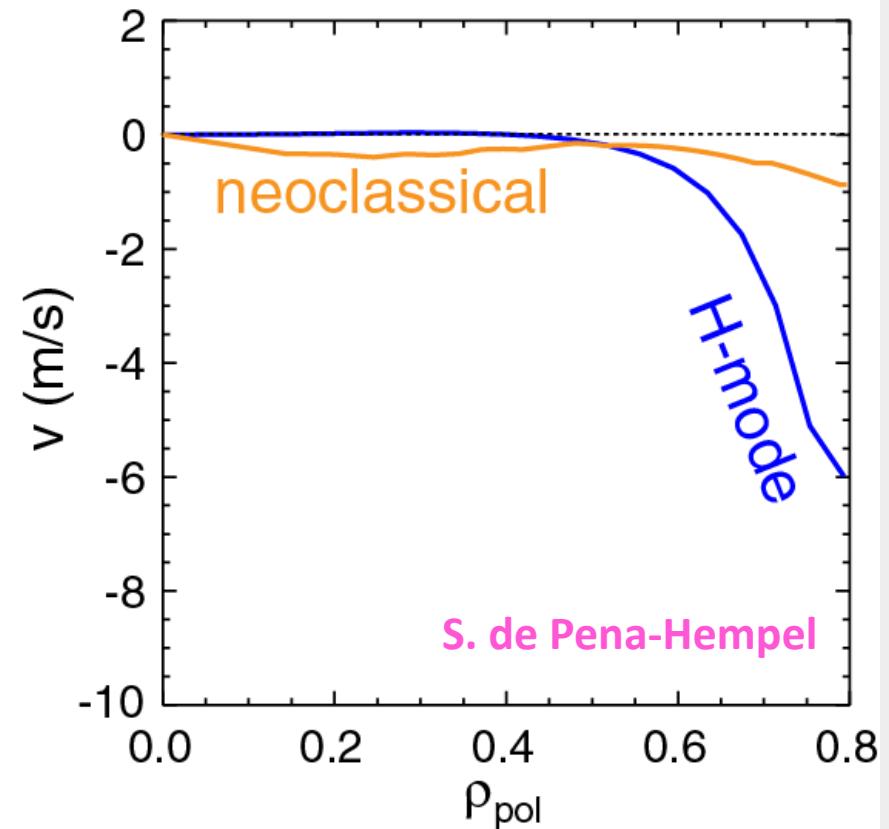
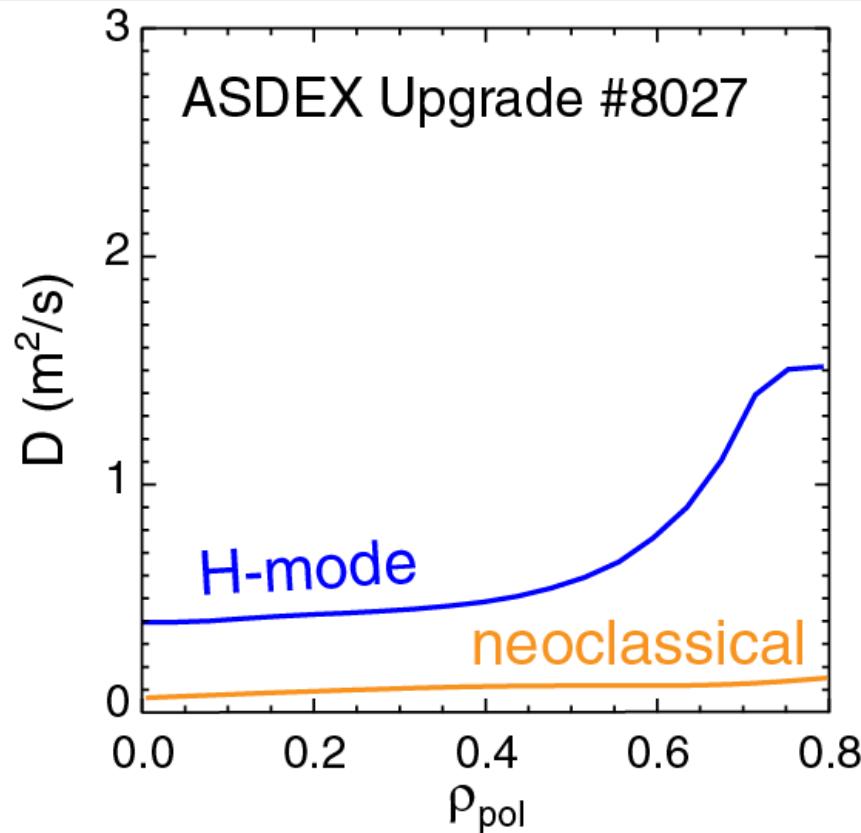
Pure neoclassical transport
leads to central impurity peaking

Peaked temperature profile
alleviates problem

Is transport really only due to collisions?

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Measure $n_z(r,t)$ after transient applied disturbance
⇒ $D(r)$ and $v(r)$



NO: "Anomalous diffusion" generally much larger!

Is "anomalous" transport good or bad?

IPP

Recall expression for impurity profile shape:

$$\frac{d \ln n_Z}{dr} = Z \frac{d \ln n_I}{dr} \left(1 + H_{eff} \frac{d \ln T}{dr} \right) \left(\frac{D}{D + D_{AN}} \right)$$

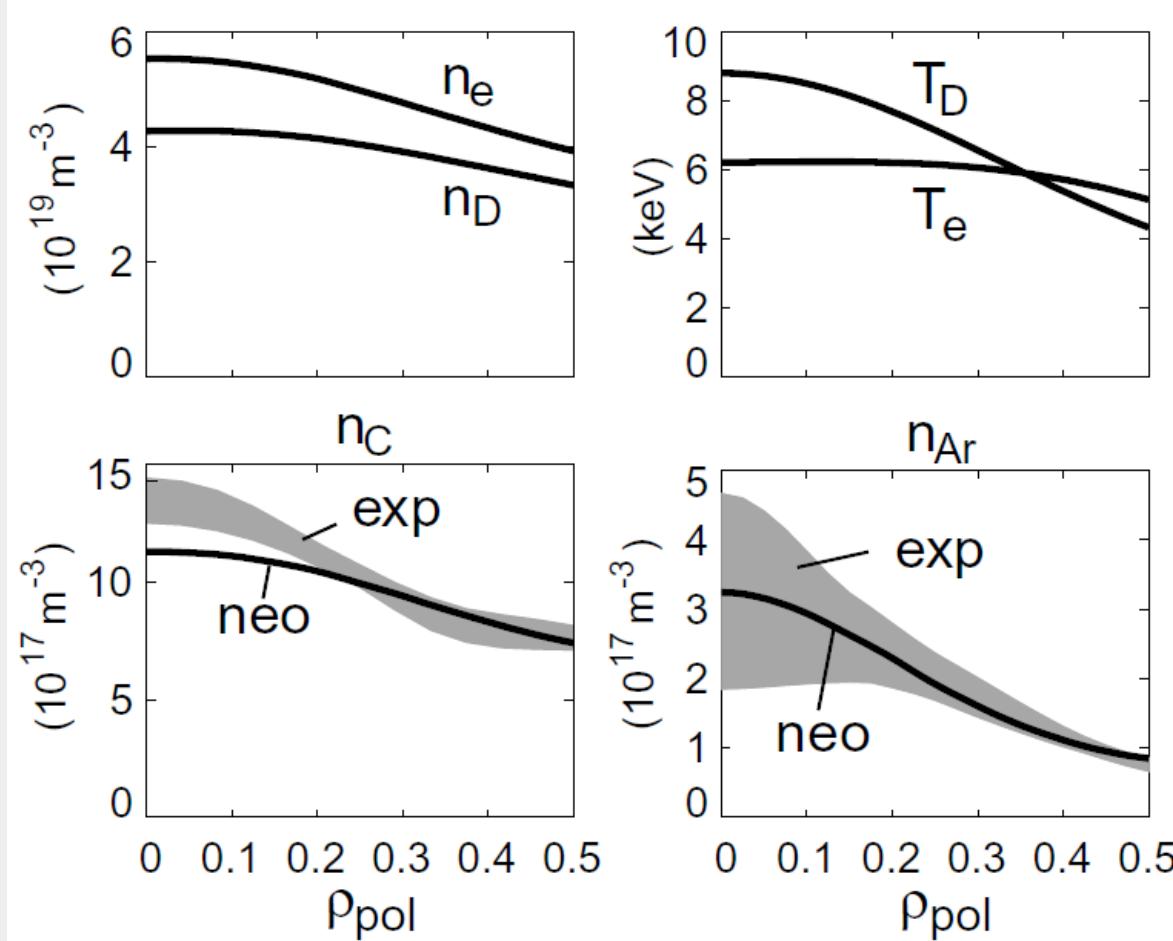
GOOD! D_{AN} decreases impurity profile peaking

Also holds for fuel ions so that $d \ln n_I/dr \downarrow$

Purely collisional transport

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Discharge with quiescent plasma



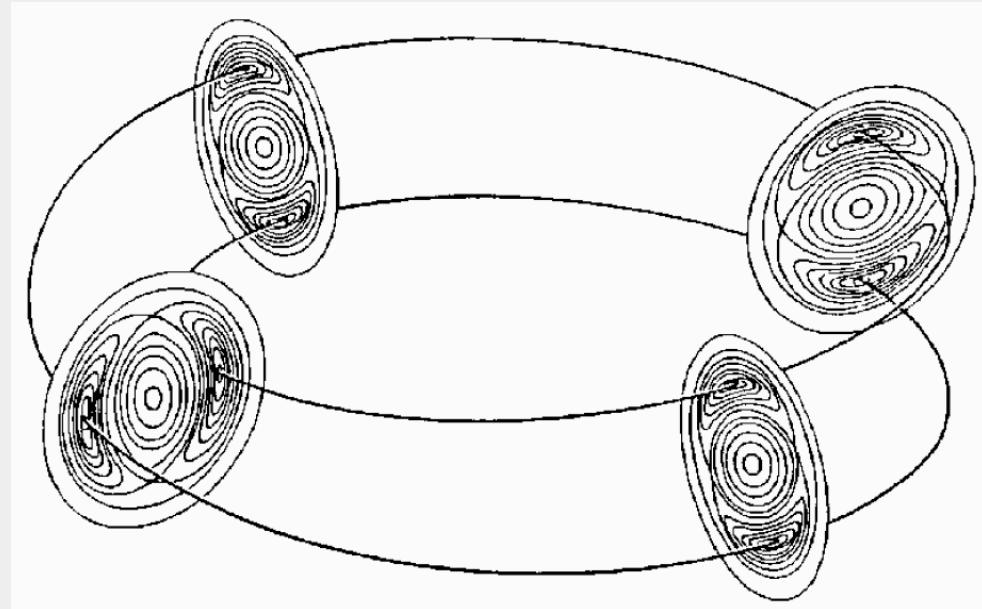
R. Dux

Impurity peaking in centre according to neoclassical D and v

What are the origins of "anomalous" transport?

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**Large scale MHD instabilities
create radial "shortcut"**

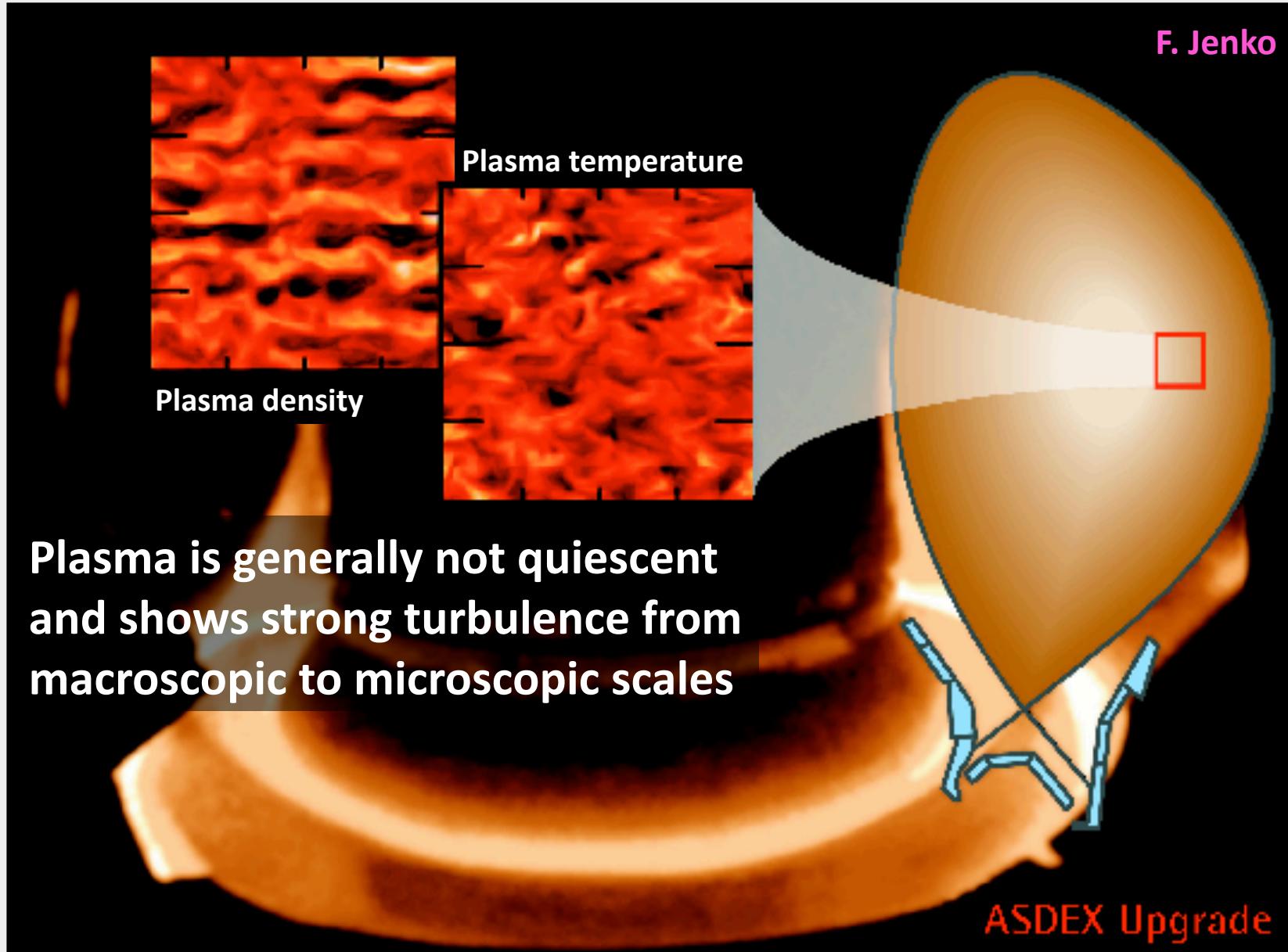


**Not the whole story:
Anomalous diffusion shows also in absence of MHD instabilities**

→ **Turbulence, carrying impurities with it!**

Turbulent processes in a Tokamak plasma?

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How can plasma turbulence be described?

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Ab initio model of plasma microturbulence
⇒ nonlinear gyrokinetic theory

F. Jenko

Hot fusion plasmas are almost collisionless (even in the edge!)

Vlasov-Maxwell equations
(self-consistent, nonlinear problem)

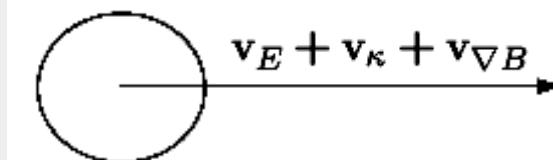
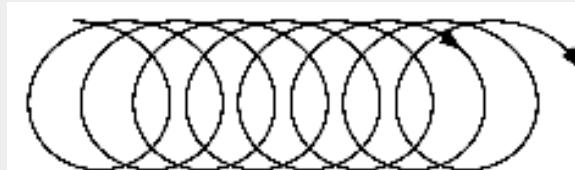
$$\left[\frac{\partial}{\partial t} + \mathbf{v} \cdot \frac{\partial}{\partial \mathbf{x}} + \frac{q}{m} \left(\mathbf{E} + \frac{\mathbf{v}}{c} \times \mathbf{B} \right) \cdot \frac{\partial}{\partial \mathbf{v}} \right] f(\mathbf{x}, \mathbf{v}, t) = 0$$

Eliminating the fast gyromotion...

$$\omega \ll \Omega$$

[Frieman, Chen, Lee, Hahm, Brizard *et al.* in the 1980s]

Charged rings as quasiparticles; important kinetic effects retained non-perturbatively!



→ Irrelevant (small) spatio-temporal scales are removed!

The nonlinear gyrokinetic equations

$$f = f(\mathbf{X}, v_{\parallel}, \mu; t)$$

advection equation/conservation law

$$\frac{\partial f}{\partial t} + \dot{\mathbf{X}} \cdot \frac{\partial f}{\partial \mathbf{X}} + \dot{v}_{\parallel} \frac{\partial f}{\partial v_{\parallel}} = 0$$

$$\dot{\mathbf{X}} = v_{\parallel} \mathbf{b} + \frac{B}{B_{\parallel}^*} \left(\frac{v_{\parallel}}{B} \bar{\mathbf{B}}_{1\perp} + \mathbf{v}_{\perp} \right)$$

$$\mathbf{v}_{\perp} \equiv \frac{c}{B^2} \bar{\mathbf{E}}_1 \times \mathbf{B} + \frac{\mu}{m\Omega} \mathbf{b} \times \nabla(B + \bar{B}_{1\parallel}) + \frac{v_{\parallel}^2}{\Omega} (\nabla \times \mathbf{b})_{\perp}$$

$$\dot{v}_{\parallel} = \frac{\dot{\mathbf{X}}}{mv_{\parallel}} \cdot (e\bar{\mathbf{E}}_1 - \mu \nabla(B + \bar{B}_{1\parallel}))$$

\mathbf{X} = position of the gyrocenter
 v_{\parallel} = parallel velocity
 μ = magnetic moment

F. Jenko

Corresponding field equations

$$\frac{n_1}{n_0} = \frac{\bar{n}_1}{n_0} - (1 - \|I_0^2\|) \frac{e\phi_1}{T} + \|x I_0 I_1\| \frac{B_{1\parallel}}{B}$$

$$\nabla_{\perp}^2 A_{1\parallel} = -\frac{4\pi}{c} \sum \bar{J}_{1\parallel}$$

$$\frac{B_{1\parallel}}{B} = - \sum \epsilon_{\beta} \left(\frac{\bar{p}_{1\perp}}{n_0 T} + \|x I_1 I_0\| \frac{e\phi_1}{T} + \|x^2 I_1^2\| \frac{B_{1\parallel}}{B} \right)$$

Nonlinear integro-differential equations in 3+2 dimensions

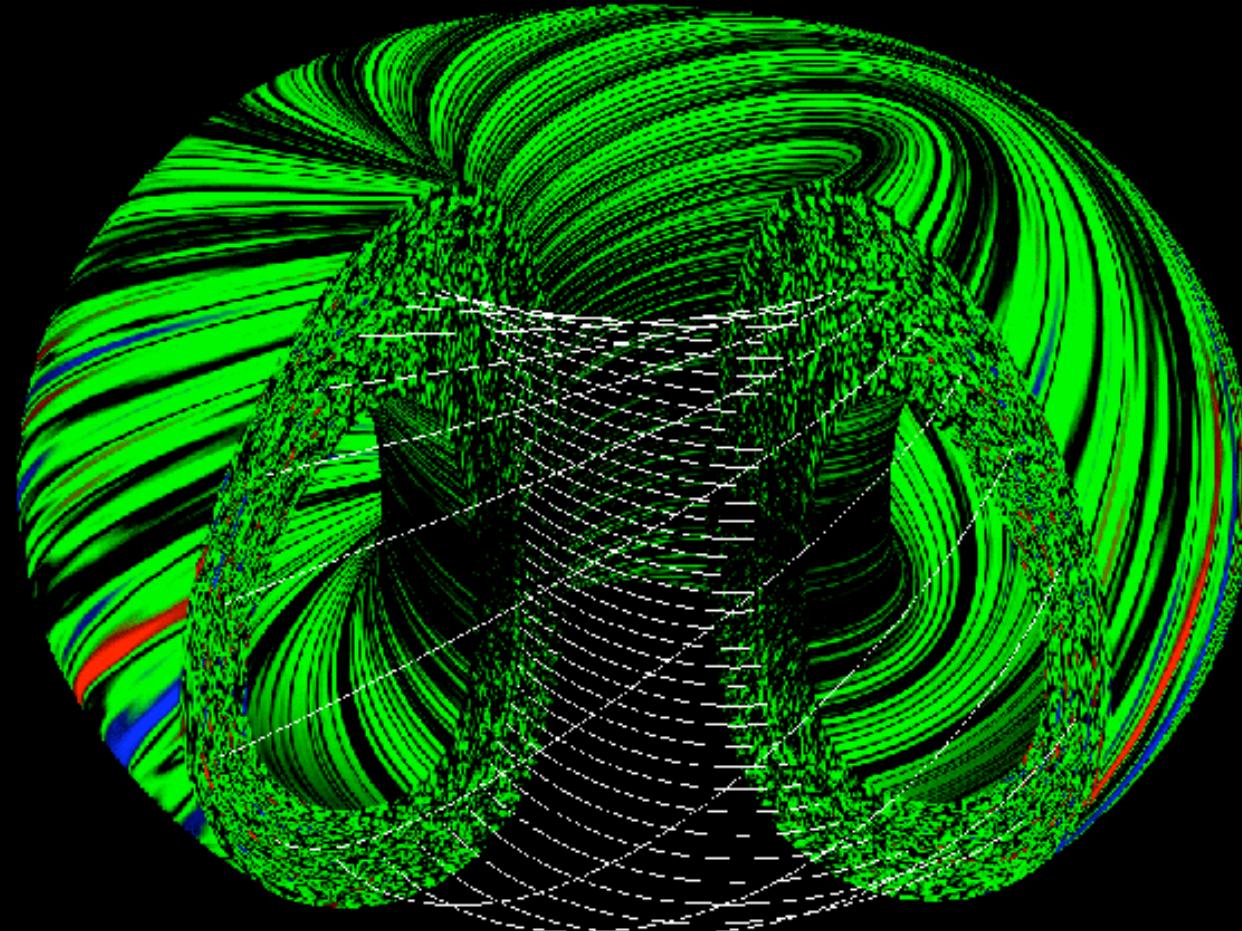
Progress only recently due to complexity of the system

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Plasma turbulence is quasi-two-dimensional



Work with flux tubes, using field-aligned coordinates



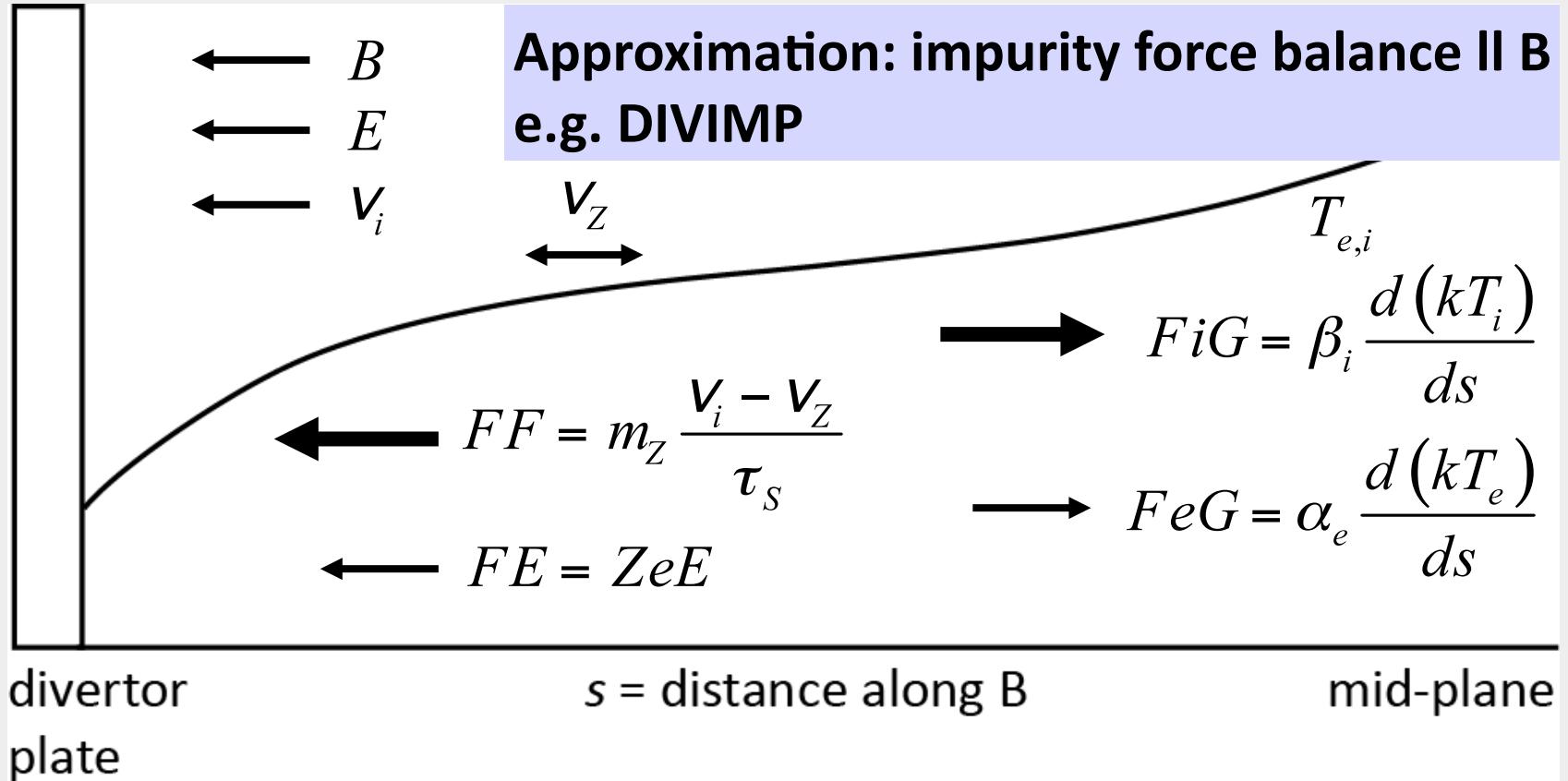
Still requires $O(100000)$ CPU-hours!

F. Jenko

Impurity transport in SOL

IPP

B-field intersects material surface  **transport II B becomes important!**



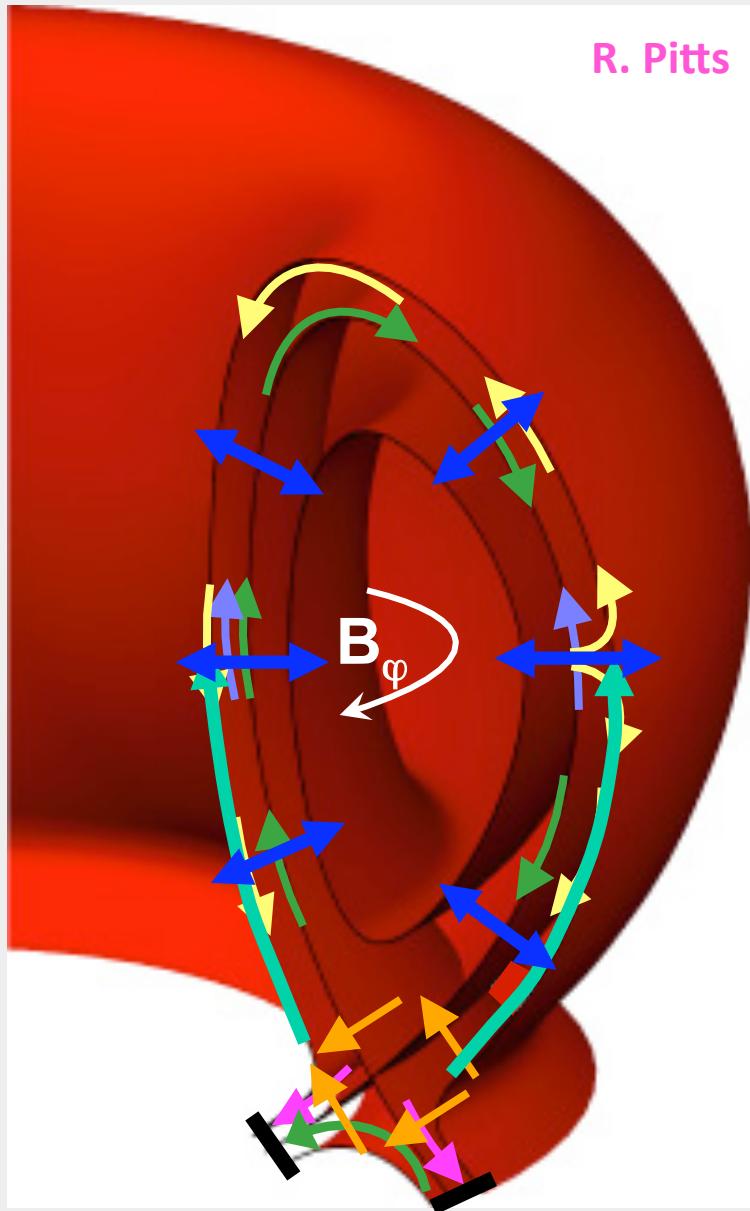
$$F_z = -\frac{1}{n_z} \frac{dp_z}{ds} + FF + FE + FiG + FeG + \dots$$

$$\tau_s \propto m_z \frac{T_i^{3/2}}{n_i Z^2}$$

$$\alpha_e \cong 0.71 Z^2$$

$$\beta_i \cong 2.65 Z^2$$

Is that the whole story?



Diffusion and
convection $\perp B$



T gradients $\parallel B$



NO: drifts & flows

$E_r \times B$, $\nabla p \times B$



$E_\theta \times B$



Pfirsch-
Schlüter



Ballooning



Divertor
sink



How to improve the quasi 1D-model?

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Kinetic equations → Moments of ion and electron distribution functions → Fluid equations
(Braginskii)

Particle balance

Momentum balance

Diffusion

Electron energy balance

Ion energy balance

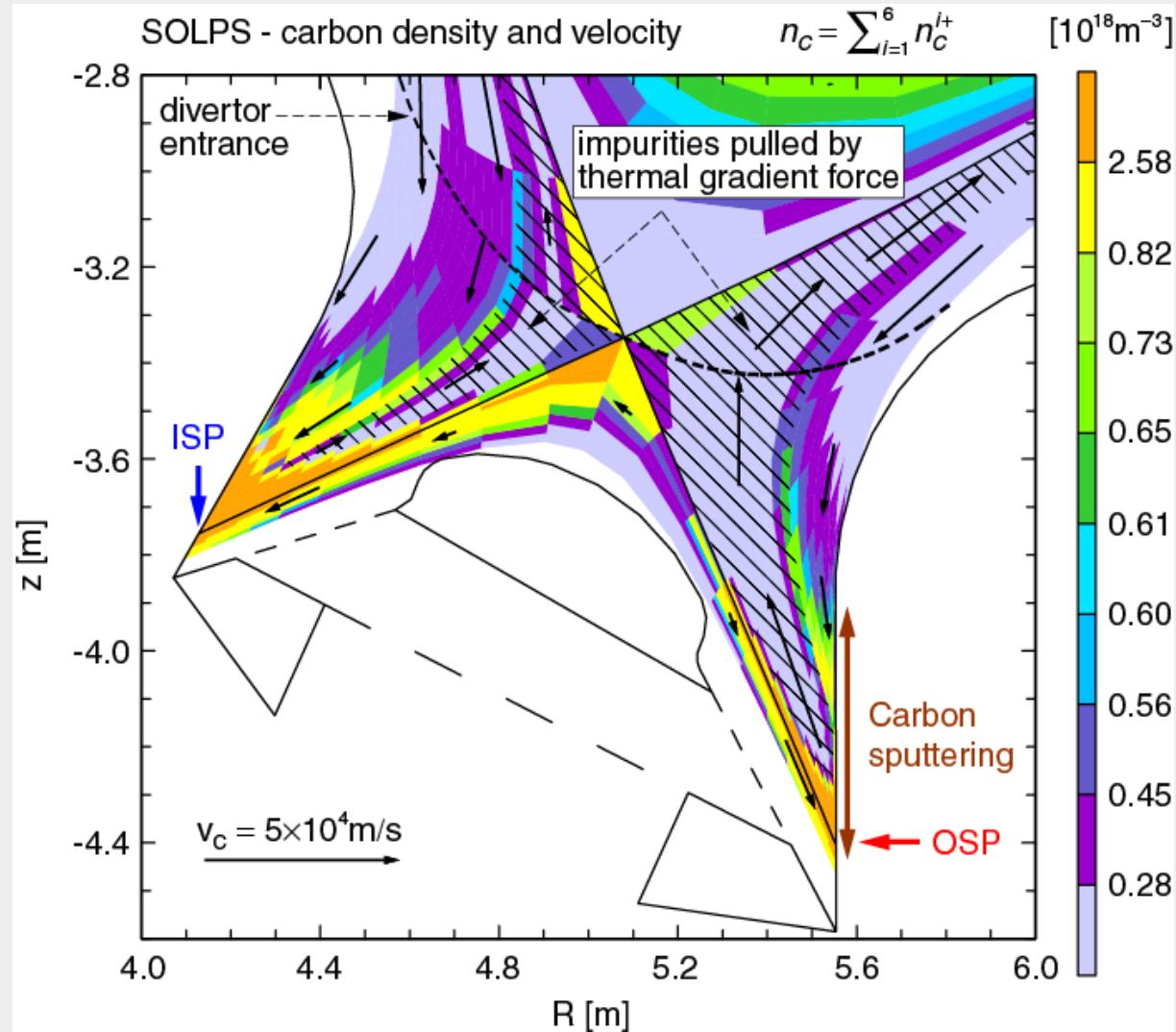
PLUS

Kinetic correction terms
(flux limiters)

Self consistent treatment of recycling
by iterative coupling to neutral transport code

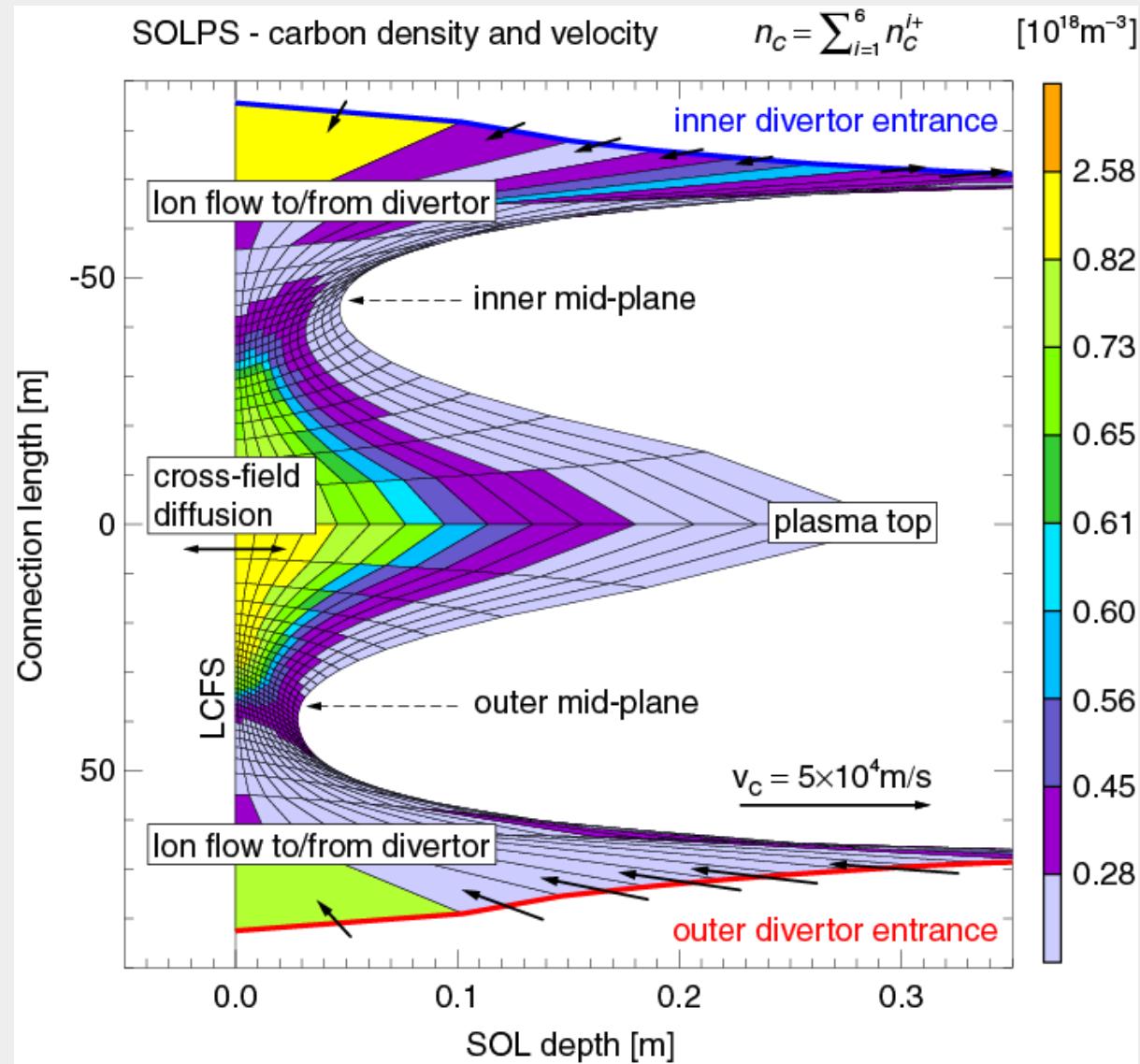
Standard used for ITER: B2-EIRENE

Example solution for ITER plasma



Example solution for ITER plasma

IPP



How to benchmark the codes?

IPP

Challenge with experimental data

Overview and rationale

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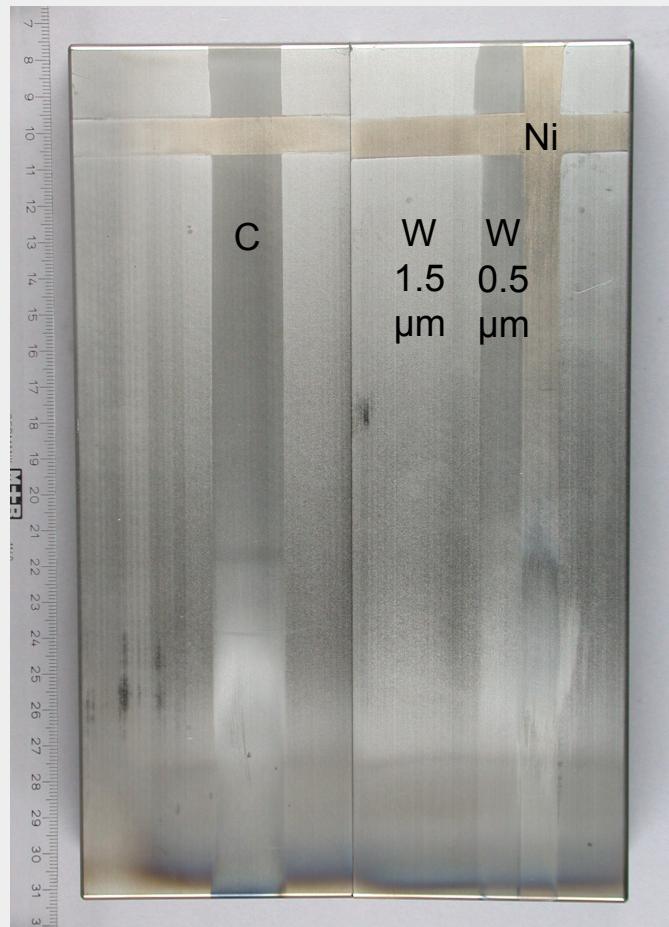
Specific experiments

Summary and outlook

**Quantify material erosion and redeposition
by ex-situ surface analysis of retrieved wall tiles
and/or long term probes**

**Identification of erosion and deposition dominated areas
Identification of net material migration balance**

Example: ASDEX Upgrade - marker tiles



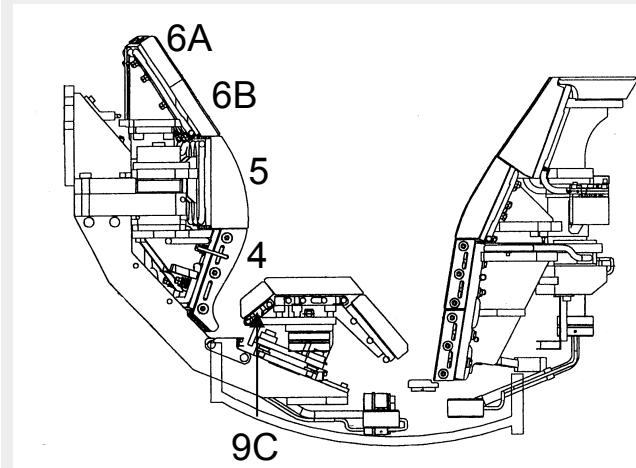
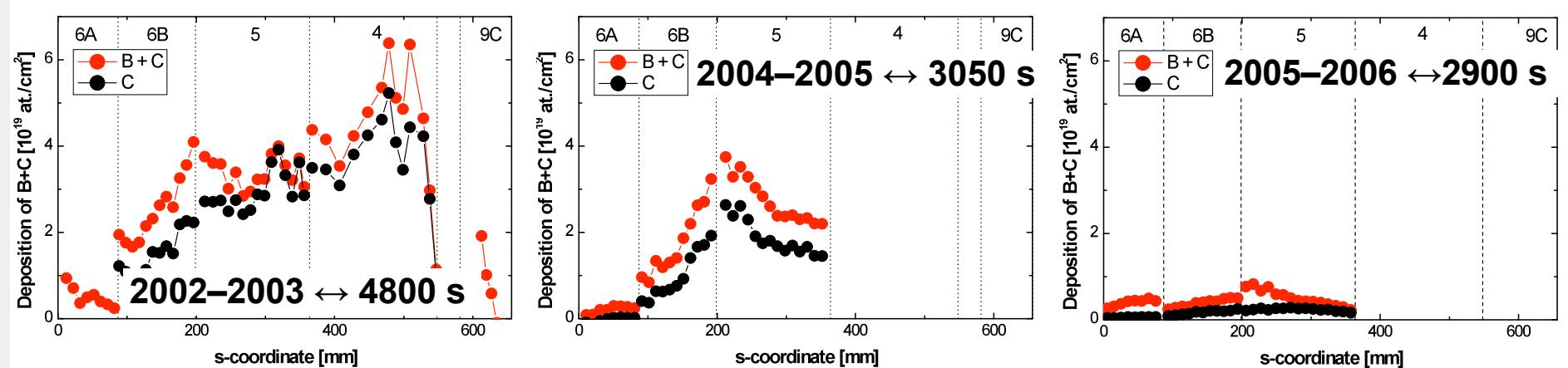
M. Mayer

Example: ASDEX Upgrade - marker tiles

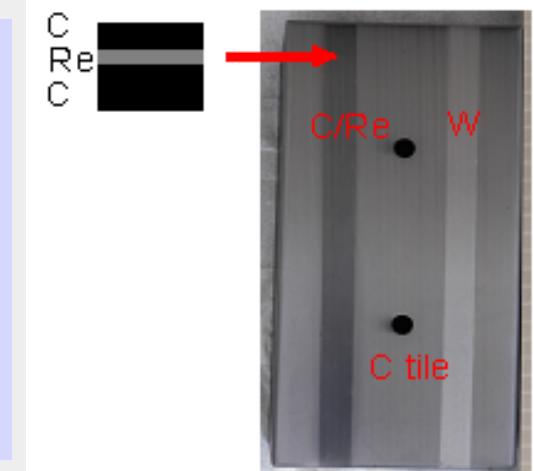
IPP

Carbon deposition in the inner divertor of ASDEX Upgrade

M. Mayer



- Decrease of C-deposition on divertor tiles by factor 7 after W coverage of outer limiters
 - No change in outer divertor erosion
- ➡ Outboard limiters identified as main carbon source

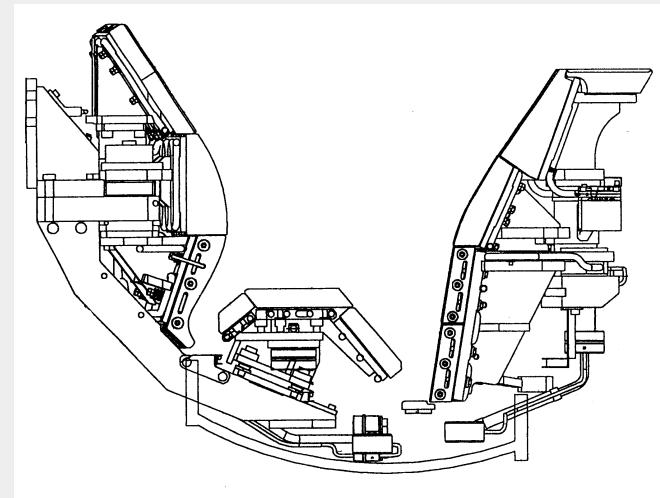
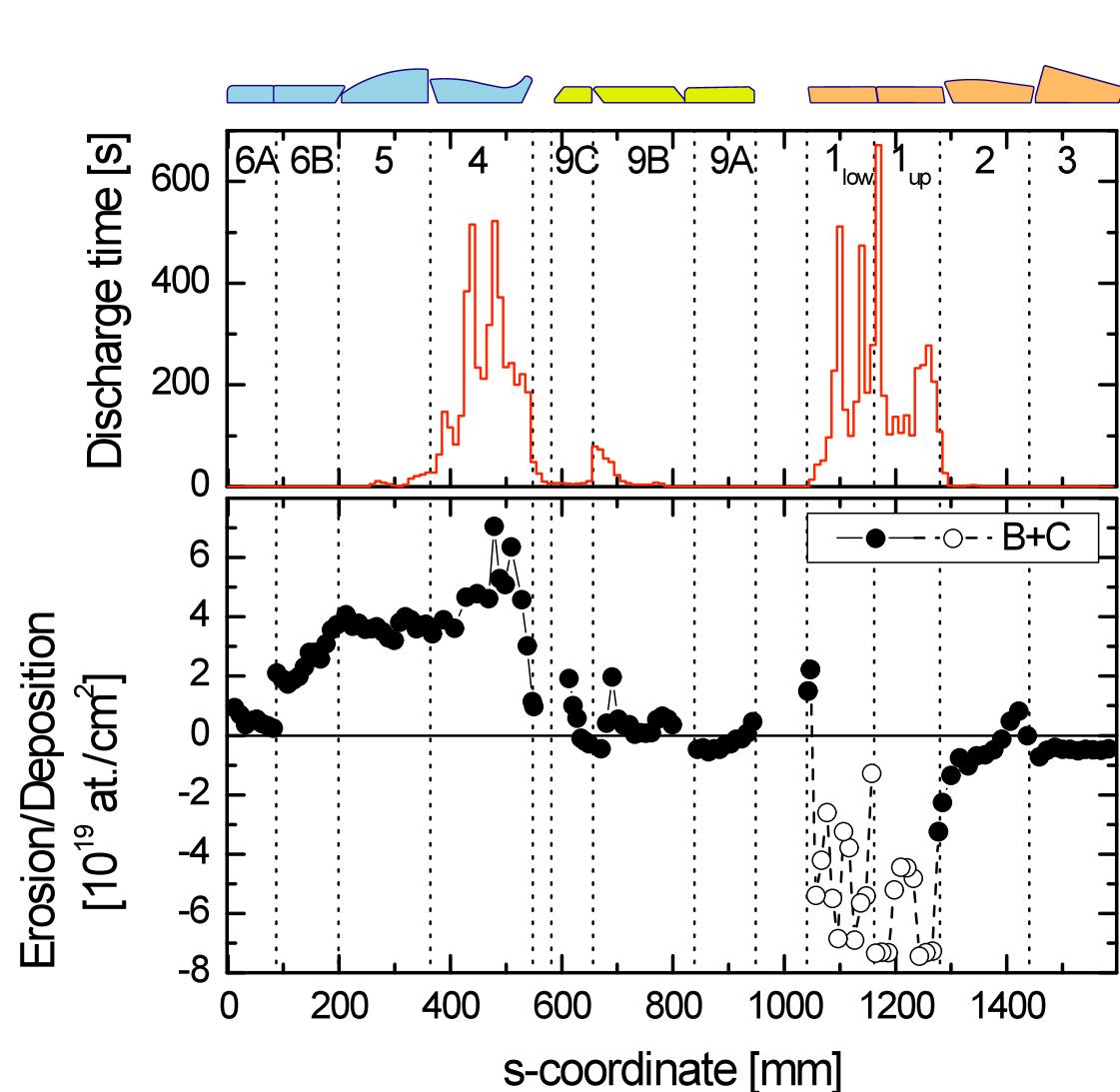


Example: ASDEX Upgrade - marker tiles

IPP

Carbon deposition / erosion in lower divertor of ASDEX Upgrade

M. Mayer

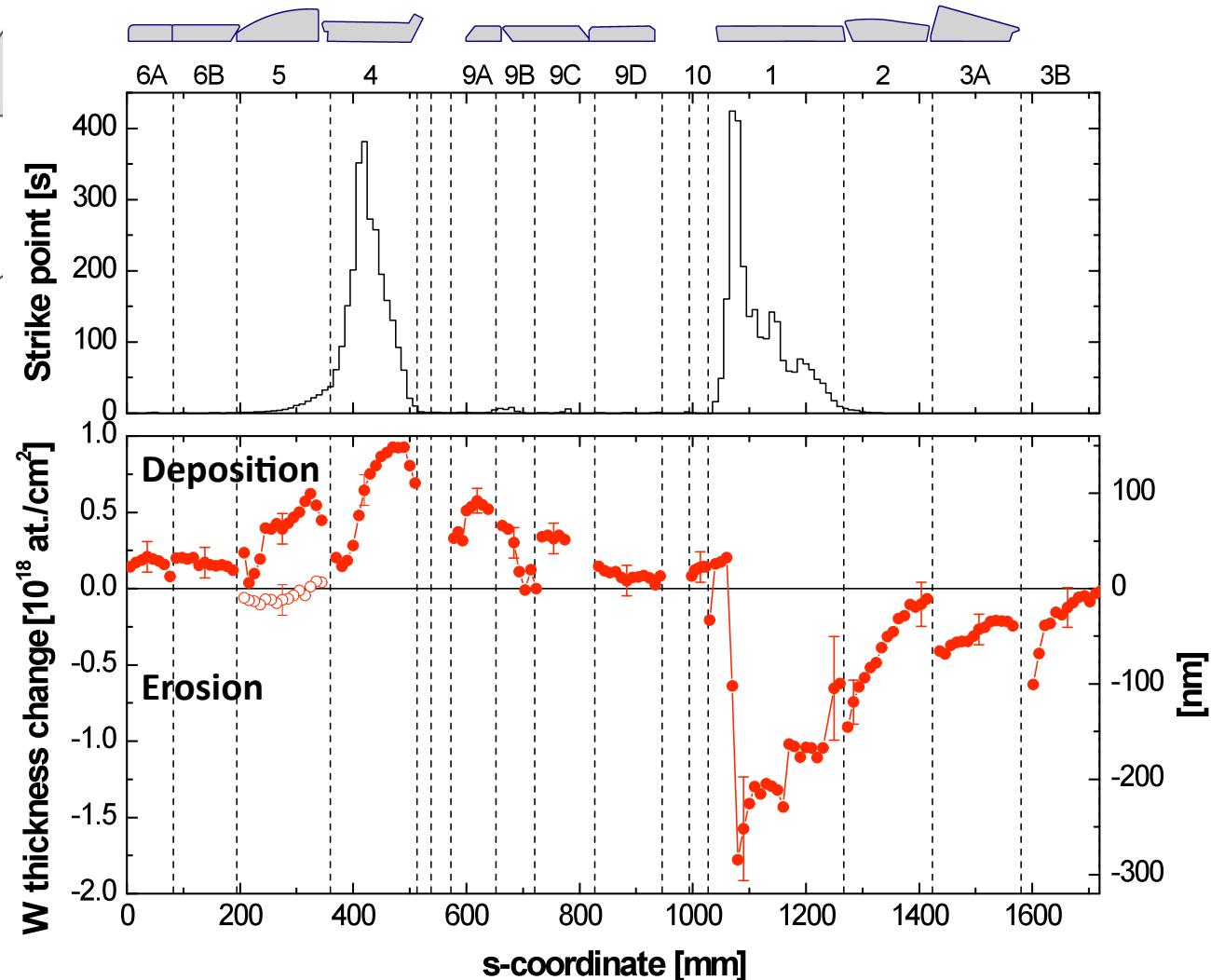
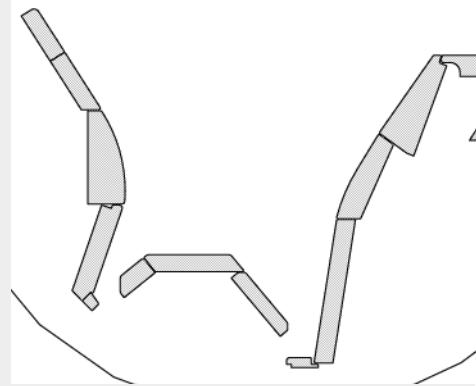


Deposition in
inner divertor
Erosion in
outer divertor

Example: ASDEX Upgrade - marker tiles

IPP

Tungsten deposition / erosion in lower divertor of ASDEX Upgrade

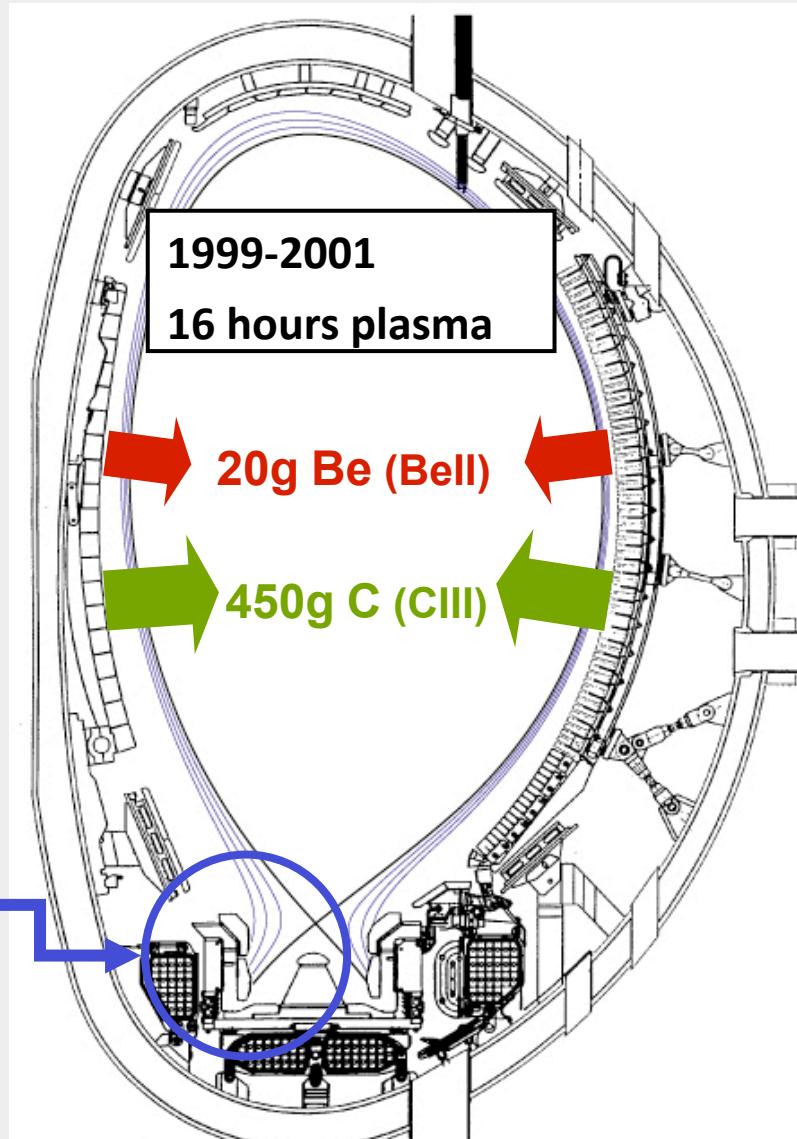
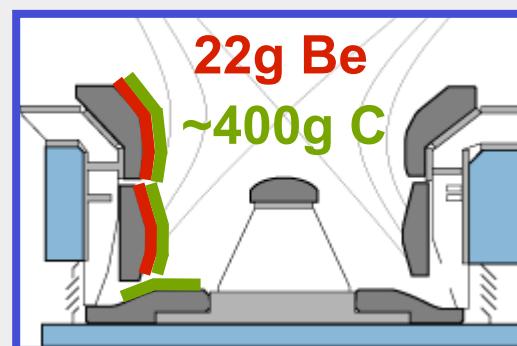


Deposition in inner divertor
Erosion in outer divertor

Example: JET accounting of Be & C erosion / deposition

IPP

- Spectroscopy + modelling
⇒ integral erosion flux
- Post mortem surface analysis
⇒ re-deposition → all at inner divertor



Likonen et al, JNM 337-339 (2005) 60, Matthews et al., EPS 2003

Advantages:

Independent of experiment programme

Possible to survey large vessel areas

Disadvantages:

Integral over many plasma scenarios makes interpretation and code benchmarking difficult

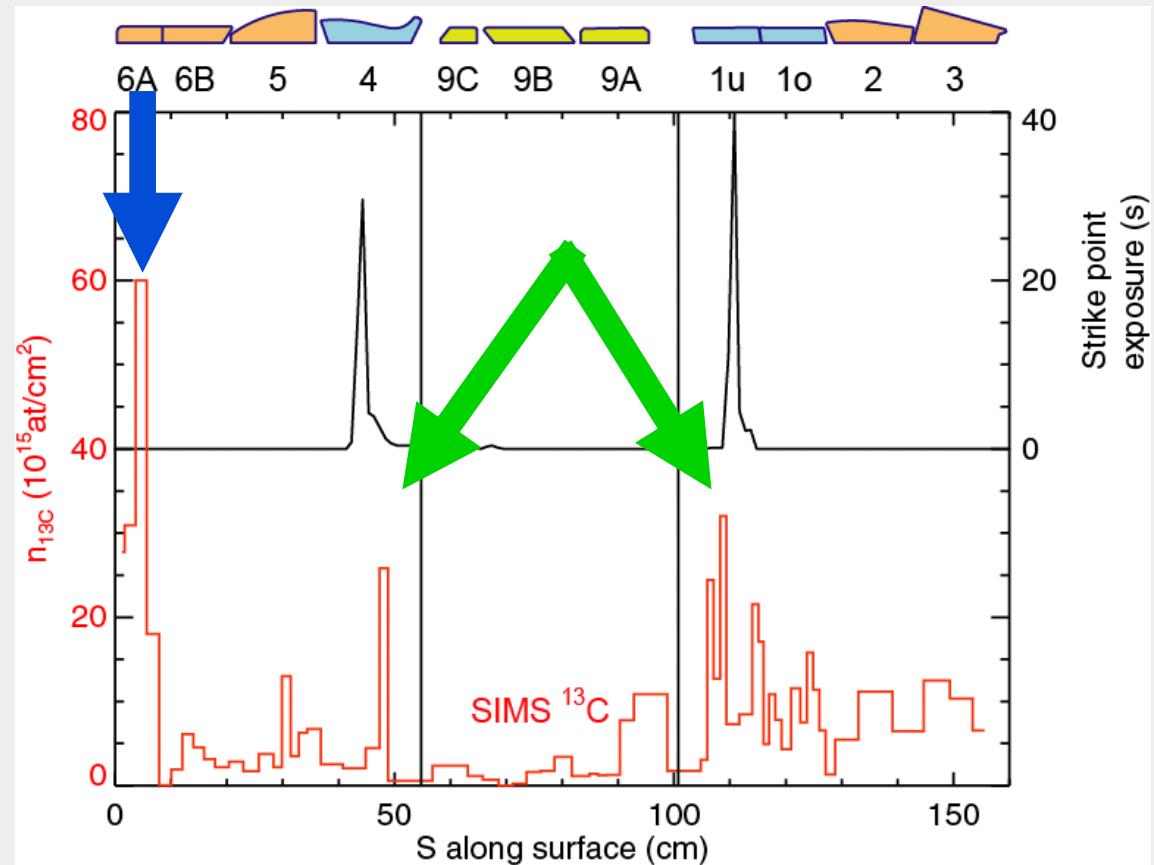
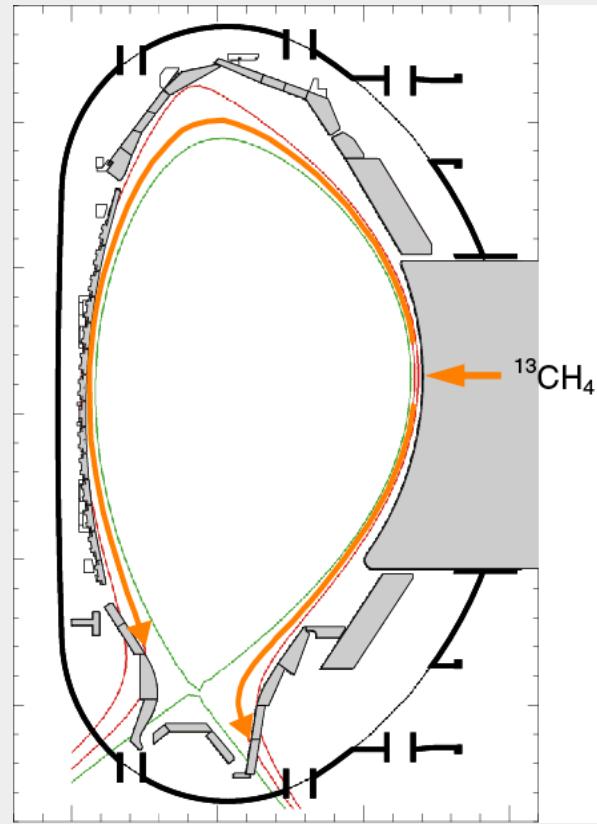
**Inject tracer material in discharges at the end
of an experimental campaign**

**Quantify tracer deposition by ex-situ surface analysis
of retrieved wall tiles and/or long term probes**

**Identification of net material migration path
(locally or globally) for particular discharge scenario**

Example: $^{13}\text{CH}_4$ injection in ASDEX Upgrade

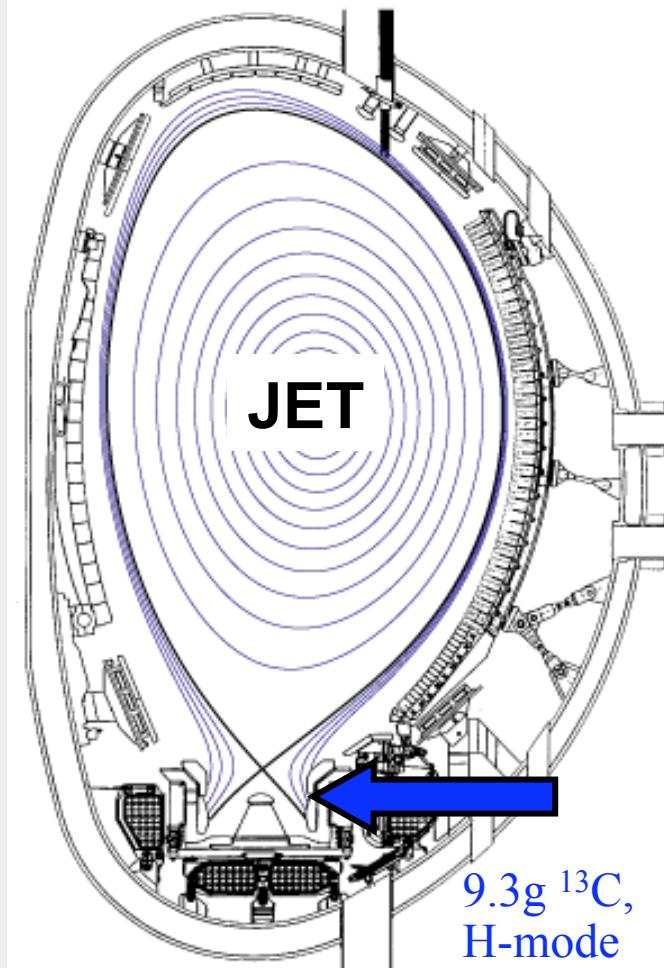
IPP



Observed deposition pattern determined by both plasma flow and by geometry

Example: $^{13}\text{CH}_4$ injection in JET

IPP

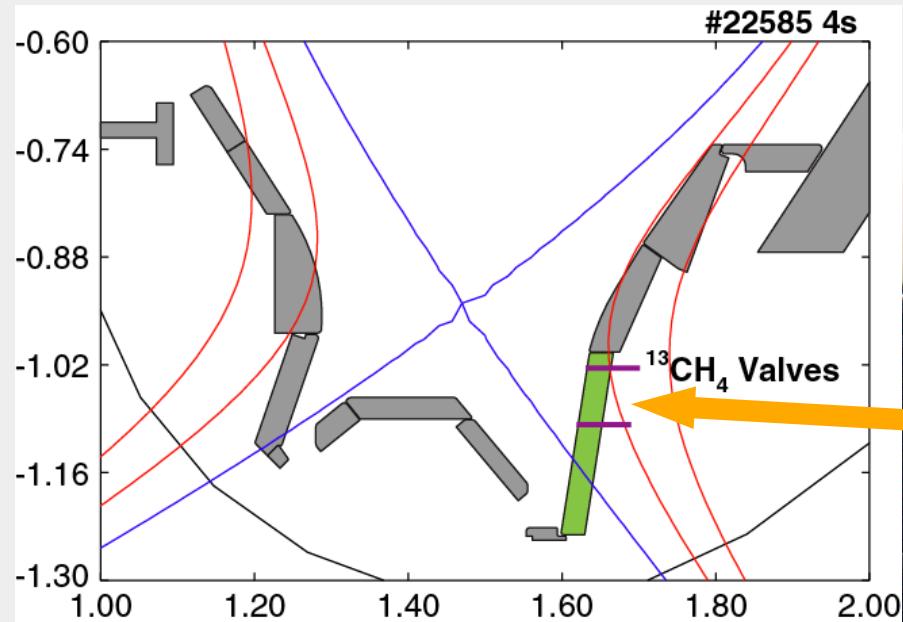


J. Strachan

Benchmarking EDGE2D fluid code model

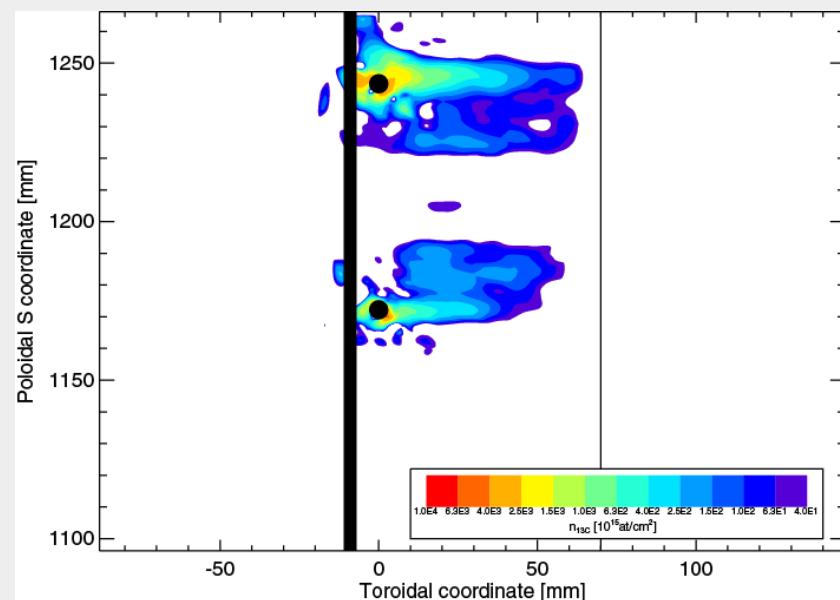
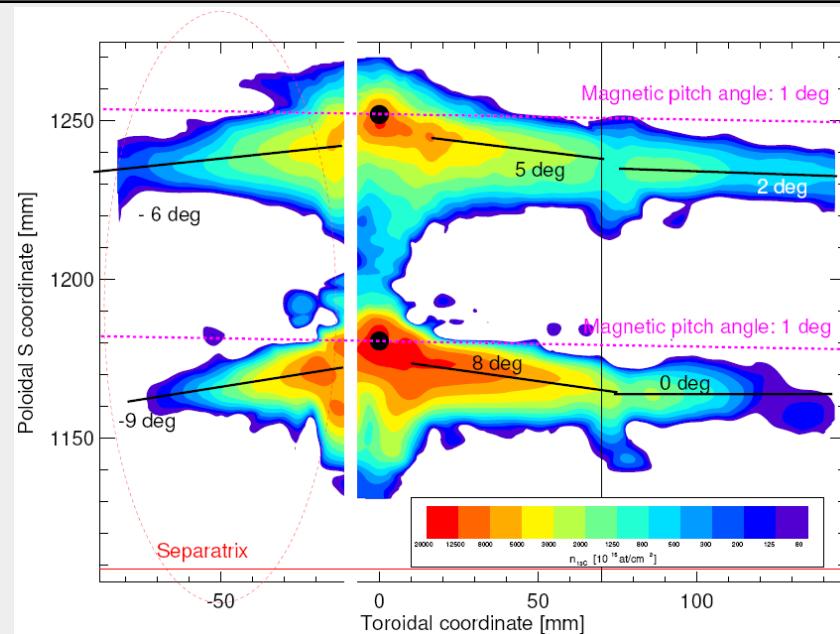
Example: $^{13}\text{CH}_4$ local injection in ASDEX Upgrade

IPP



- Puff trace amounts of $^{13}\text{CD}_4$ in series of similar discharges and measure local ^{13}C deposition 2D-distribution at retrieved tiles.
- Benchmark data for ERO and for spectroscopic CD flux measurements

Example: 13CH₄ local injection in ASDEX Upgrade



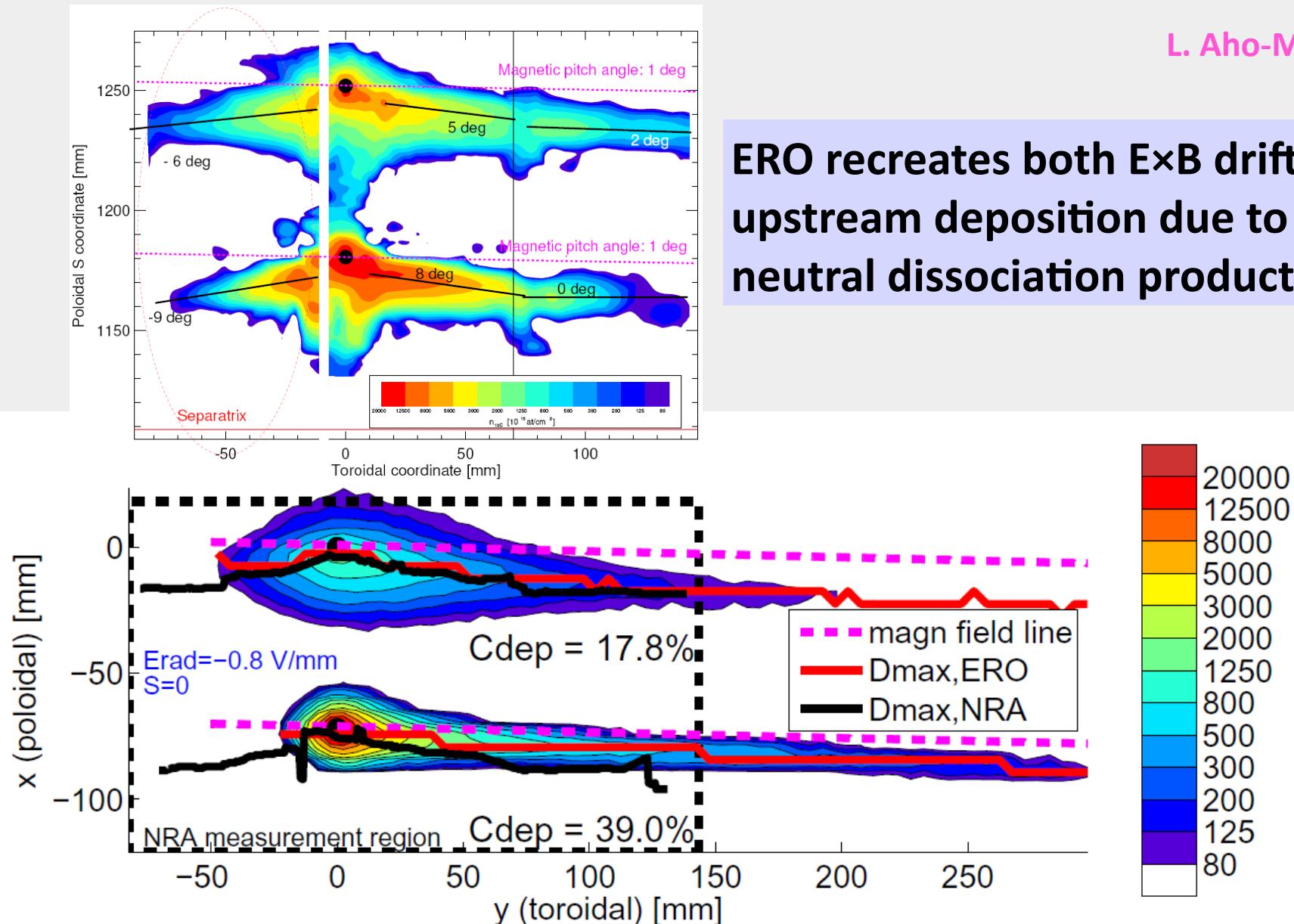
- 11 L-mode discharges
- ¹³CH₄ puff 1.6–4.6 s

Reversal of deposition shift at
B-field reversal
Shift due to ExB drift

- 3 L-mode discharges
- ¹³CH₄ puff 1.6–4.3 s
- Reversed B_t, I_p

Example: 13CH₄ local injection in ASDEX Upgrade

L. Aho-Mantila



ERO recreates both $E \times B$ drift and upstream deposition due to neutral dissociation products

Advantages:

Well defined particular discharge scenario for code benchmarking

Very sensitive quantification of tracer materials

Disadvantages:

Provides only net-deposition data. Re-erosion only by indirect evidence

Only one scenario per campaign

Cover main chamber wall with Be by heavy Be evaporation.

Follow relaxation of Be/C wall sources, plasma concentration and QMB deposition towards steady state situation.

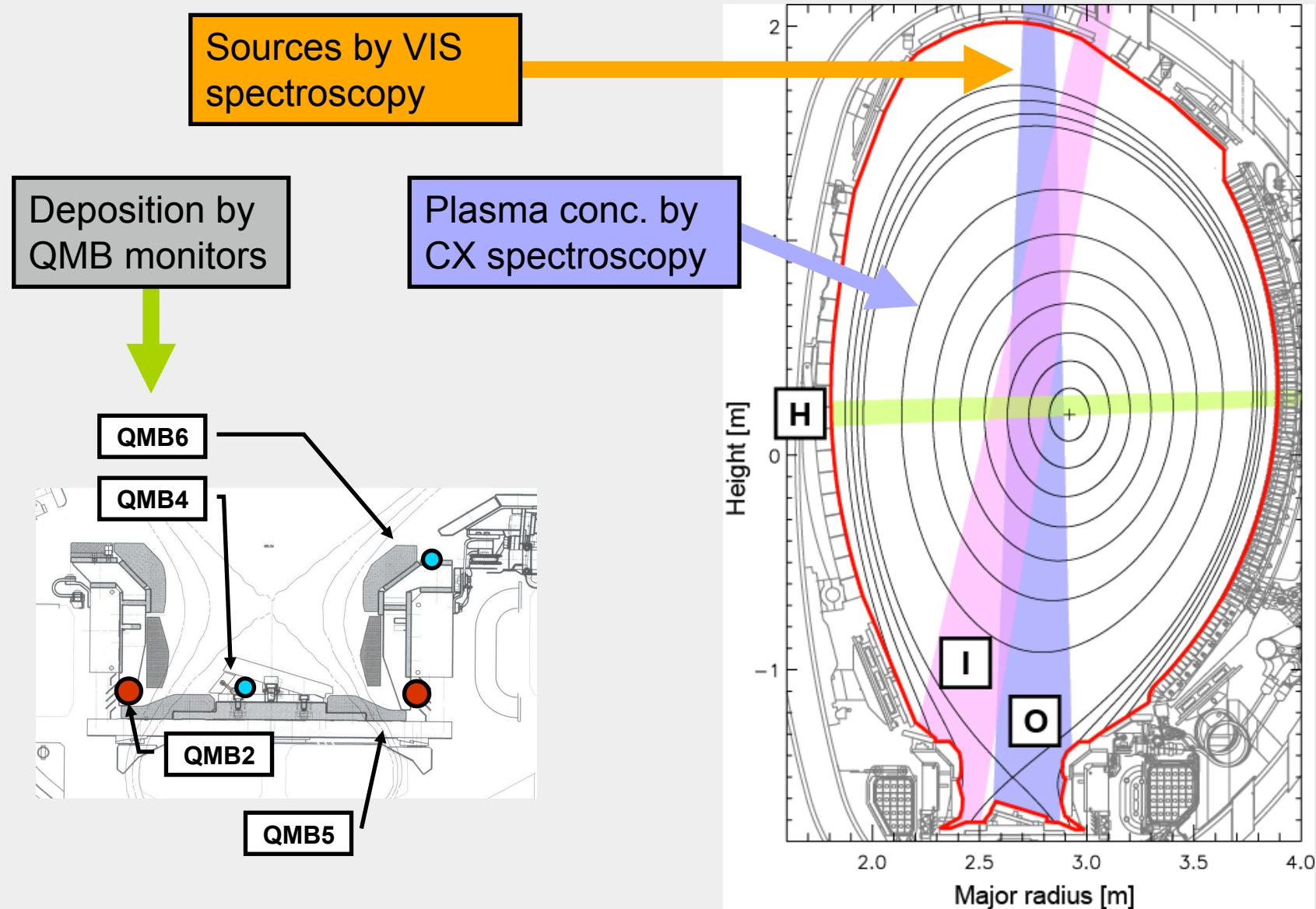
Compare to reference discharge immediately before Be evaporation.

Spectroscopic measurements allow to determine gross erosion flux.

Allows to study global screening by comparison with plasma impurity concentration.

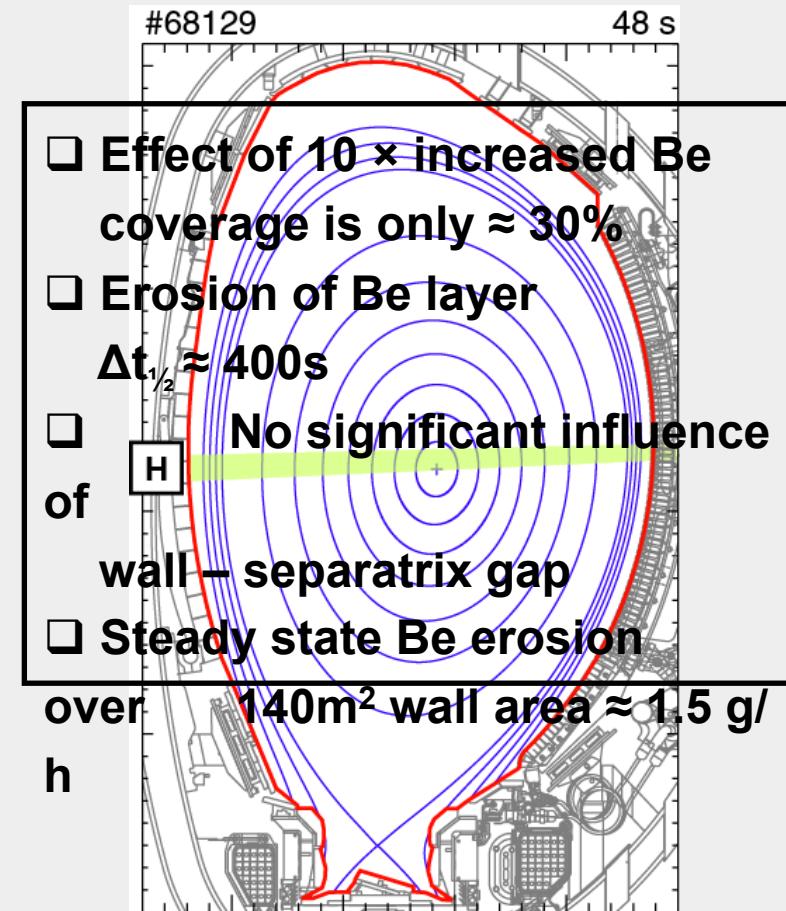
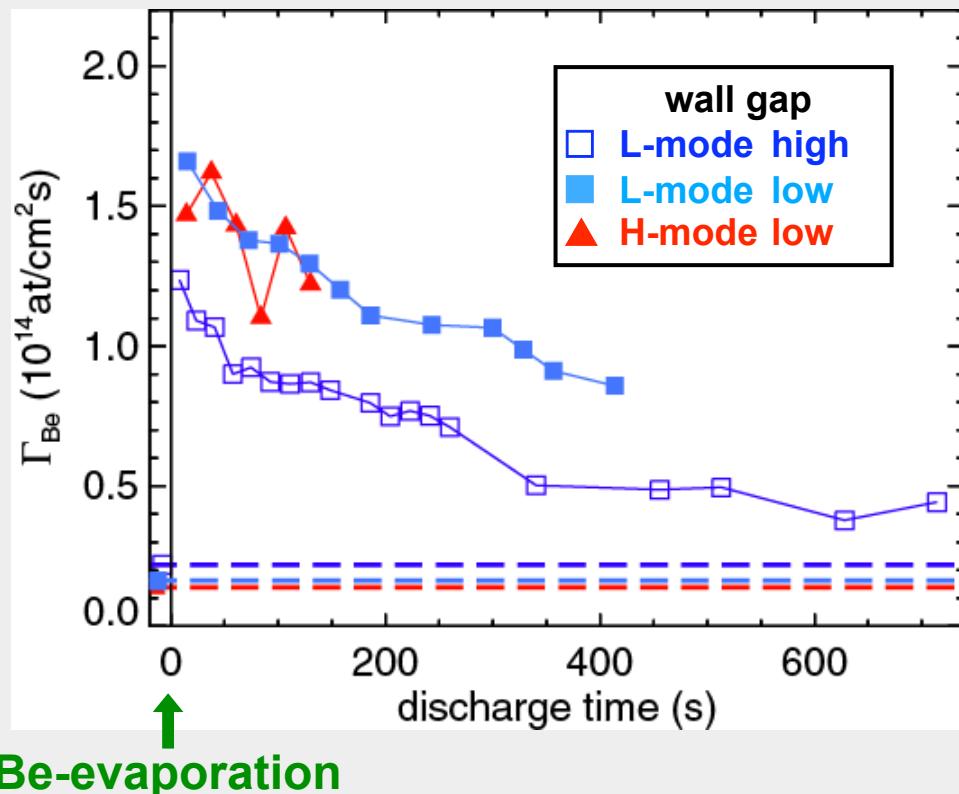
Evolution of wall composition provides information on material migration.

Diagnostic array



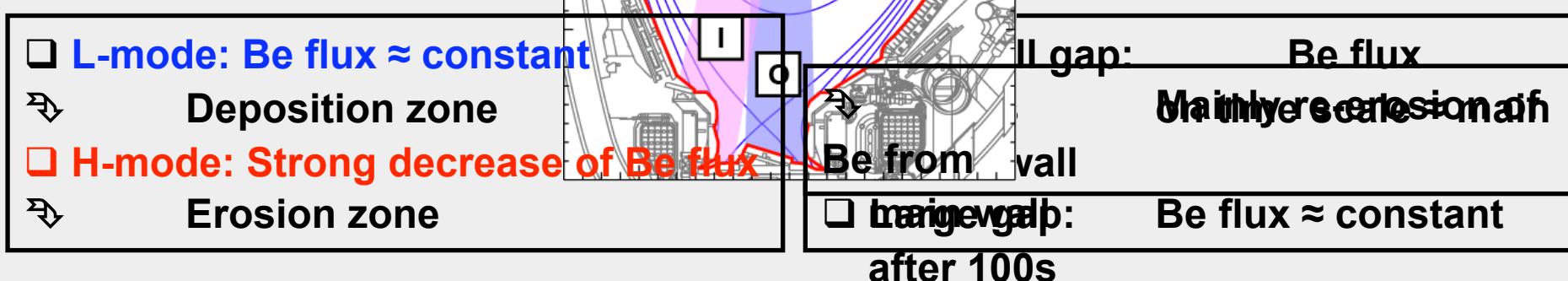
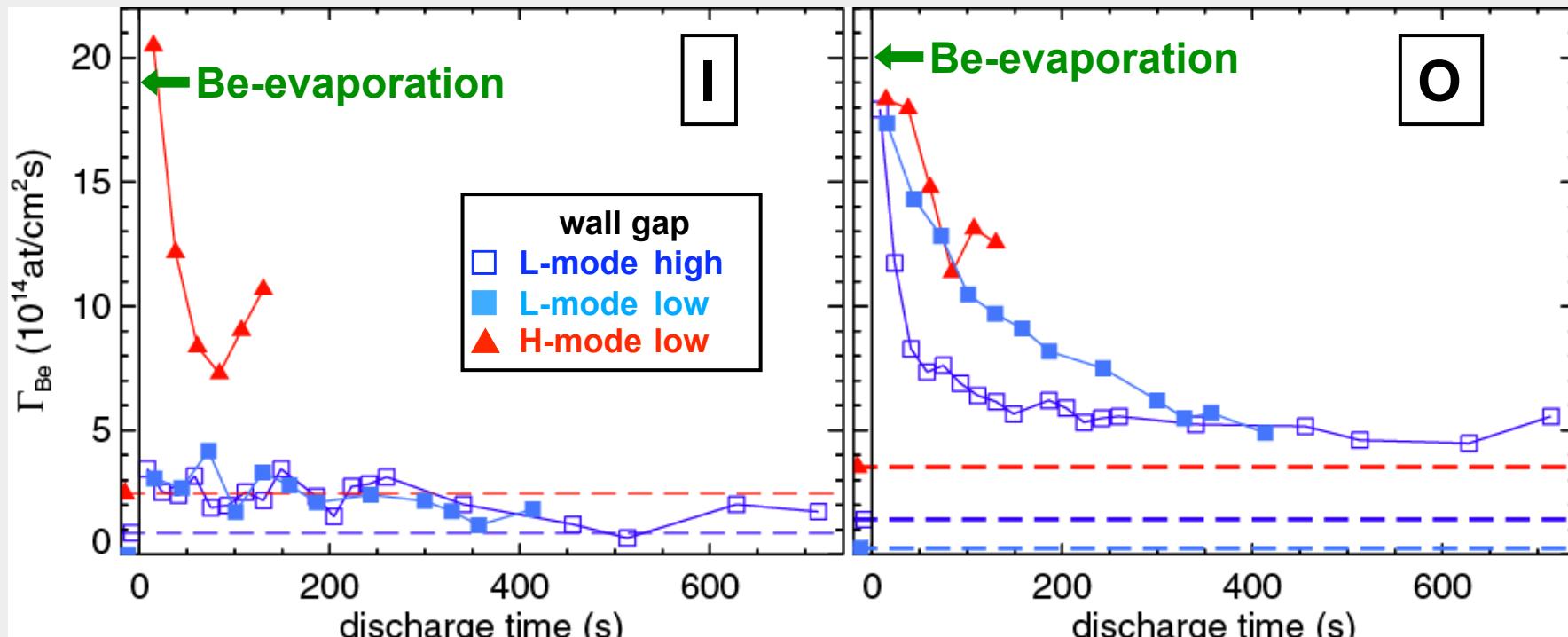
Evolution of Be wall sources

Local Be flux at first wall mid-plane from Be II line (527nm)



Evolution of Be divertor sources

Integrated Be flux from inner (I) and outer (O) divertor from Be II (527nm)



Modelling wall composition change by migration

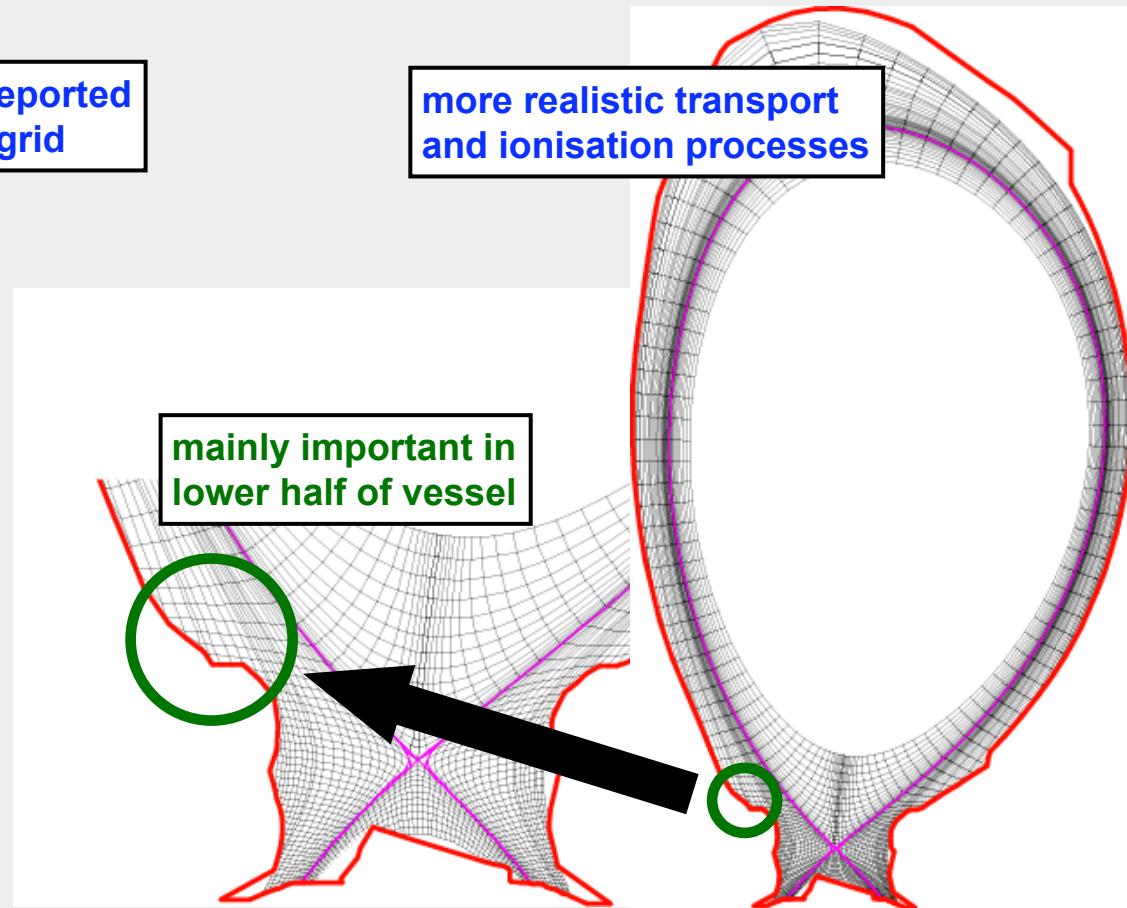
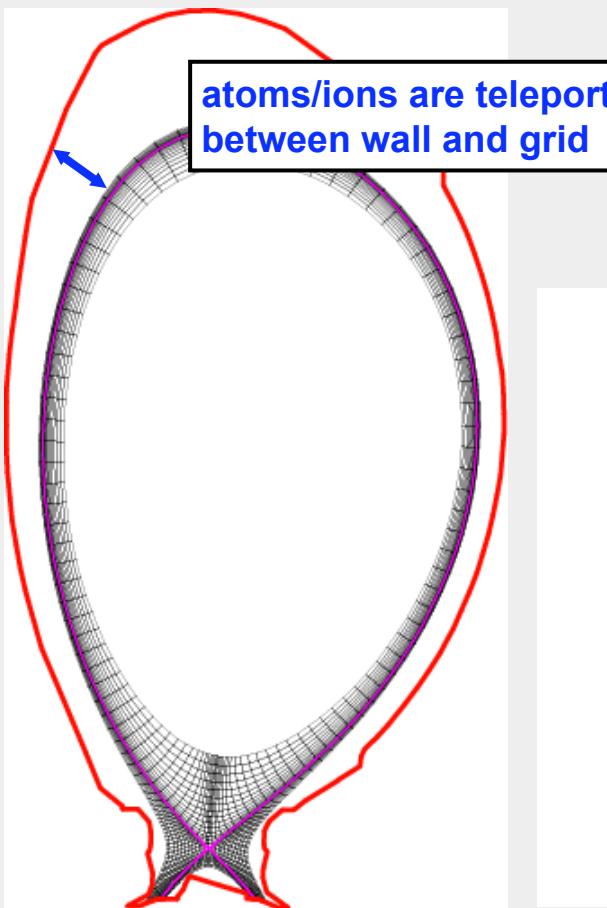
IPP

- Standard grid topology is restricted to plasma-wall contact at target plates

⇒ Missing processes at "white spots":

- \parallel and \perp transport to wall
- ionisation & transport of eroded atoms

- Extend grid and tailor to 1st wall
- Fill with plasma using extrapolation from original grid



Advantages:

- Well defined particular discharge scenario for code benchmarking
- Trace several materials simultaneously

Disadvantages:

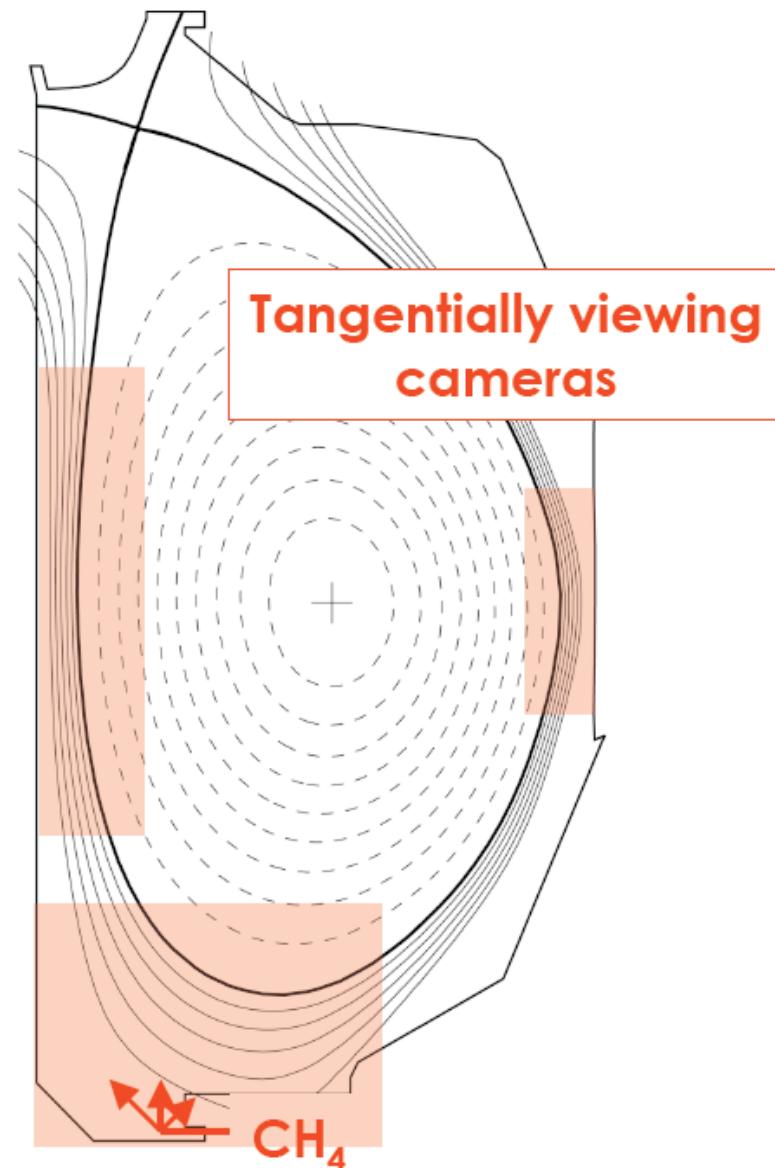
- Provides only gross erosion data. Deposition only by indirect evidence
- Quantitative impurity flux quantification requires local plasma parameters

Direct observation of impurity radiation during injection

Spectroscopic measurements allow to determine spatial distribution of emission by successive ionisation states

Allows to directly observe the influence of transport

Example: carbon flow measurements in DIII-D



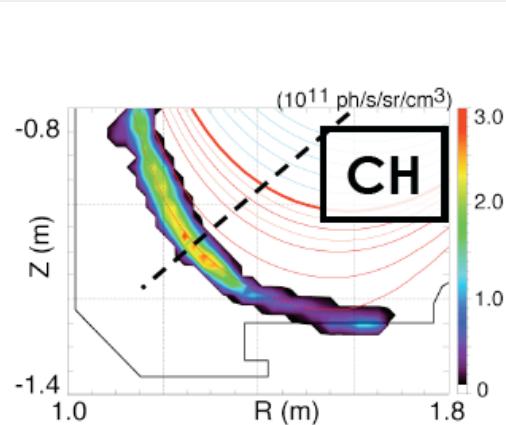
- **Principal flow measurements in the plasma crown**
 - Multi-tipped, reciprocating Langmuir probe: parallel- \mathbf{B} v_{D+}
 - Passive Doppler spectroscopy: parallel- \mathbf{B} v_{C+}, v_{C2+}
- **Toroidally symmetric injection of CH₄ from lower outer pumping plenum + tangential cameras**
 - Emission profiles: direction of low charge-state carbon flow
 - Order-of-magnitude estimate of C⁺ poloidal velocity

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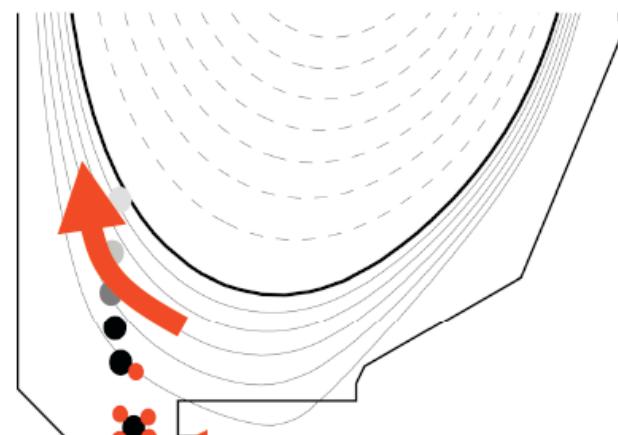
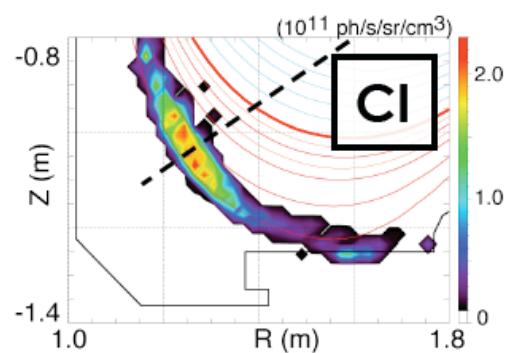
Example: carbon flow measurements in DIII-D

IPP

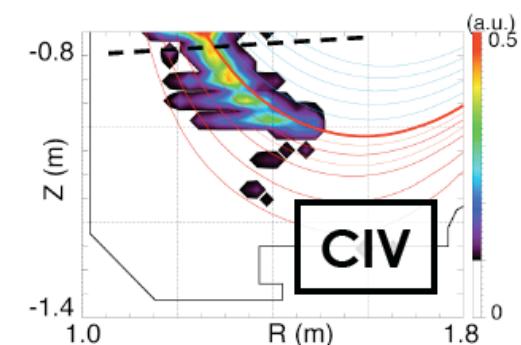
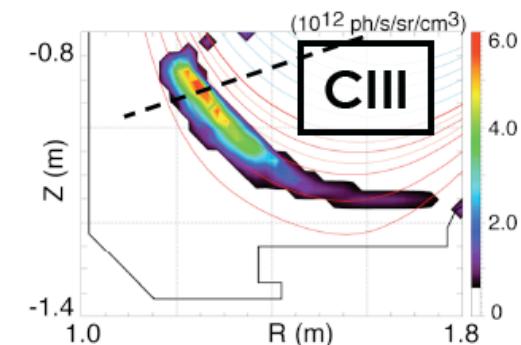
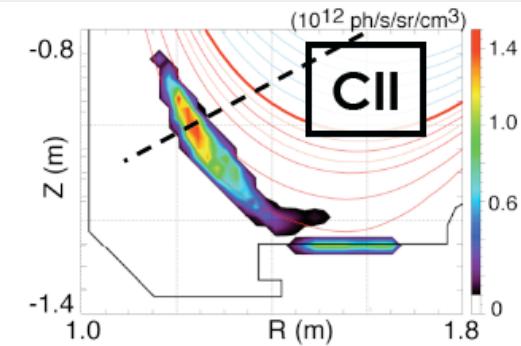
Carbon emission profiles of CH₄ break-up are progressively shifted radially inward and poloidally toward inner plate



M. Groth



CH₄ injection



Overview and rationale

Material transport processes

Particle collisions

Plasma turbulence

Experiments

Phenomenological observations

Specific experiments

Summary and outlook

Experiment side

**Implement new PSI and impurity transport diagnostics
to study timedepepent processes in single discharges**

Improve diagnostics for characterisation of incident plasma flux

Modelling side

Get complete treatment of transport processes

Coupled codes for plasma and material side

Extend computational domain for plasma towards entire 1st wall

Develop 3D codes for near wall domain